



# Integrated Modeling

**What is it?**  
**What does it do for NGST?**  
**What do we do well?**  
**What can we do better?**

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## What is Integrated Modeling ?

- To many, this term is simply synonymous with multi-disciplinary analysis and simulation
- This is (all too?) often limited to the so-called “forward modeling problem”, where we model a design, model the loads acting upon the system, model the constraints, etc. and “turn the crank”
- Examples:
  - perform design/requirements verification (example: error budget “bottoms-up” analysis, i.e. margin prediction)
  - perform sensitivity analysis and MDO (multidisciplinary design optimization), albeit often in an awkward and ad-hoc manner
  - simulate output of one system/process for input to another (example: synthetic imagery used to develop/test ground-based software for image post-processing)
  - labs & testbeds: hardware emulation, real-time control
- After 6 years “in the business”, my conclusion is that we should apply a broader meaning to the word integrated than this, but let’s save that for later...



## Aside: Concepts of Validation and Verification



- Ref: John Azzolini, “Essential Systems Engineering: A Lifecycle Process”, 1995
- Validation relates to formulation. Answer the question: “Did I build the right model?” A validated model has been shown to properly address the question, issue, requirement, etc. for which it was built. Critical to this process is a thorough vetting of the underlying assumptions, methods, and tools.
- Verification relates to implementation. Answer the question: “Did I build the model right?” A verified model has been shown to accurately parameterized, be “bug-free”, etc. Ideally, such a model can accurately predict performances, under a variety of conditions, which are confirmed via hardware test. Sometimes, a model can’t be verified until after we launch and deploy.



# **NGST Modeling Examples: “Yardstick” and “Nexus” studies (circa 1996-2000)**



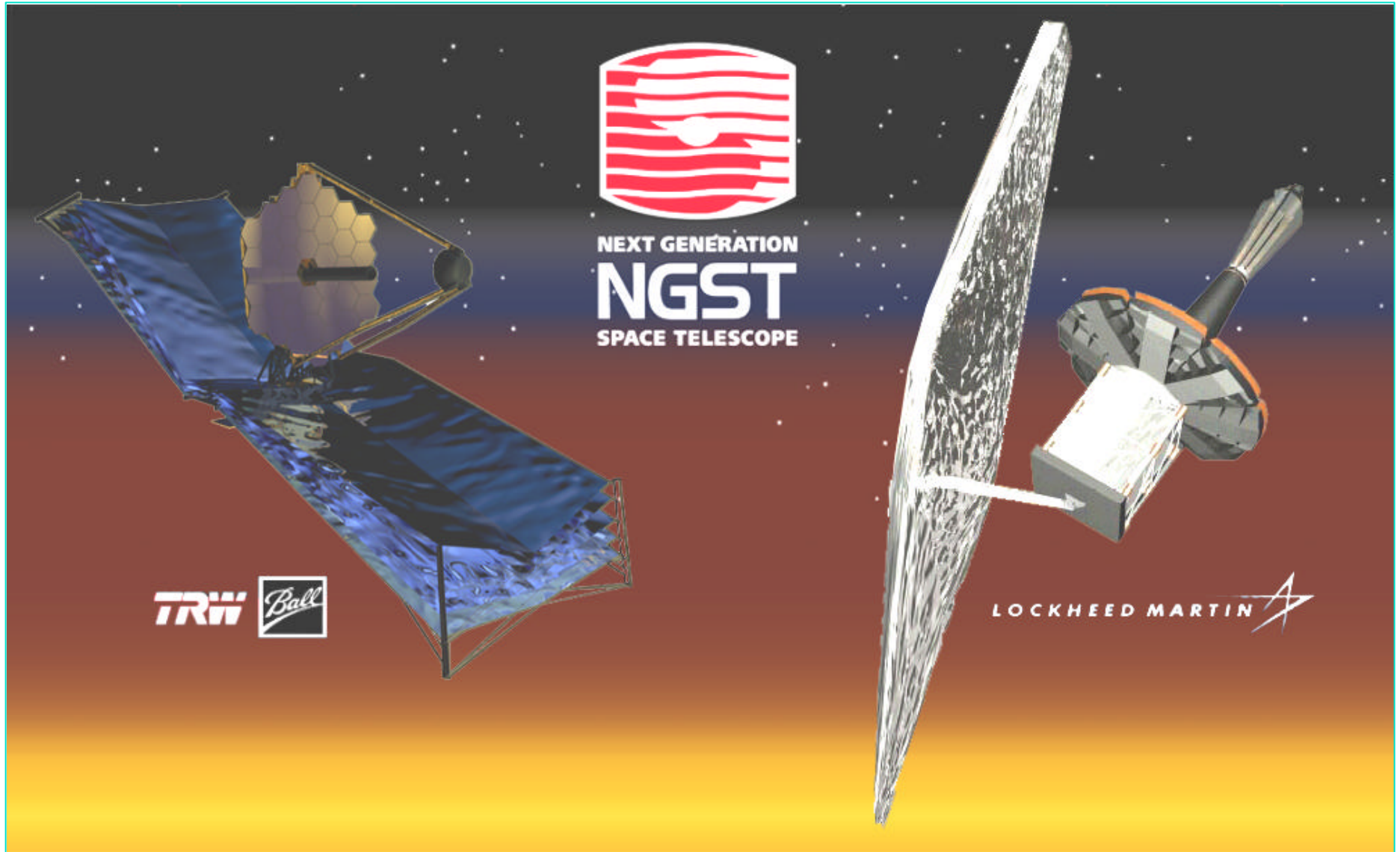
# NGST Overview



- **Part of the ORIGINS program, the follow-on to Hubble Space Telescope**
- **Significant work started at GSFC in 1996, currently transitioning between formulation and implementation phases**
- **Present focus is on major procurements:**
  - **Prime contractor for optical telescope assembly, sunshield, and systems integration**
  - **Instruments and detectors**
  - **Additional contributions from international partners**
    - **ESA: spacecraft and instrument technology**
    - **CSA: fine guidance sensor and instrument technology**
- **Milestones: PDR 2003, CDR 2004, Launch 2009**



# Industry Concepts





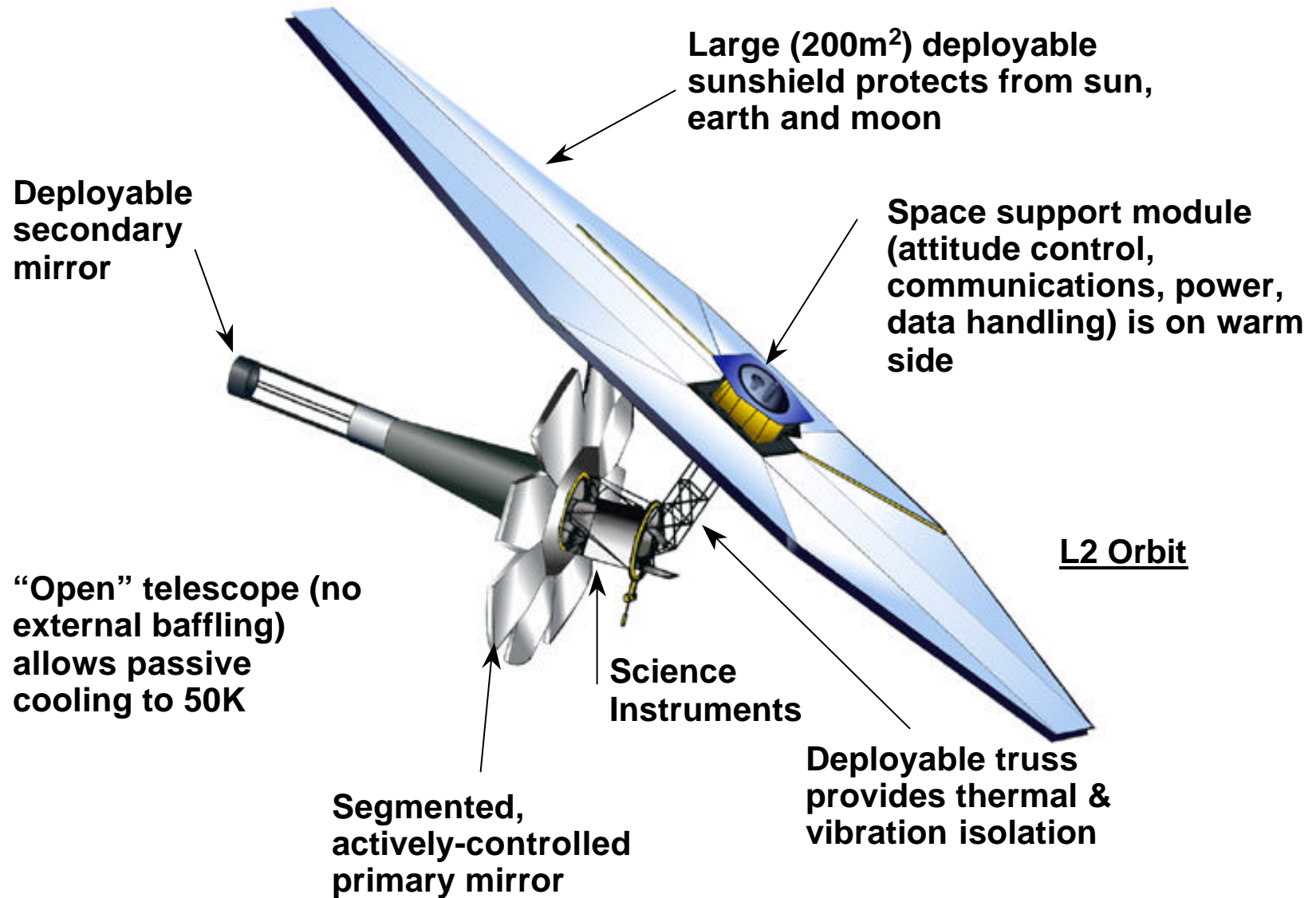
## Key Science Drivers



- **Mission objectives: study the large scale geometry of the universe, the origin of galaxies, and the nature of the earliest generations of stars**
- **Near-infrared optimized to study red-shifted galaxies**
- **Sensitivity requirement for faint-object detection (specifies point source flux as function of wavelength, filter bandpass, integration time, and signal-to-noise ratio)**
- **Image quality and stability requirements for resolution and operational efficiency**
  - **Diffraction-limited at 2 micron wavelength (Strehl ratio of 0.8)**
  - **Encircled Energy fraction GTE 75% within 150 mas radius at 1 micron wavelength**
  - **EE stable within +/- 2% over 24 hour period, and similarly stable between major recalibrations**



## NGST “Yardstick” Concept







# Integrated Modeling throughout the Project Life Cycle



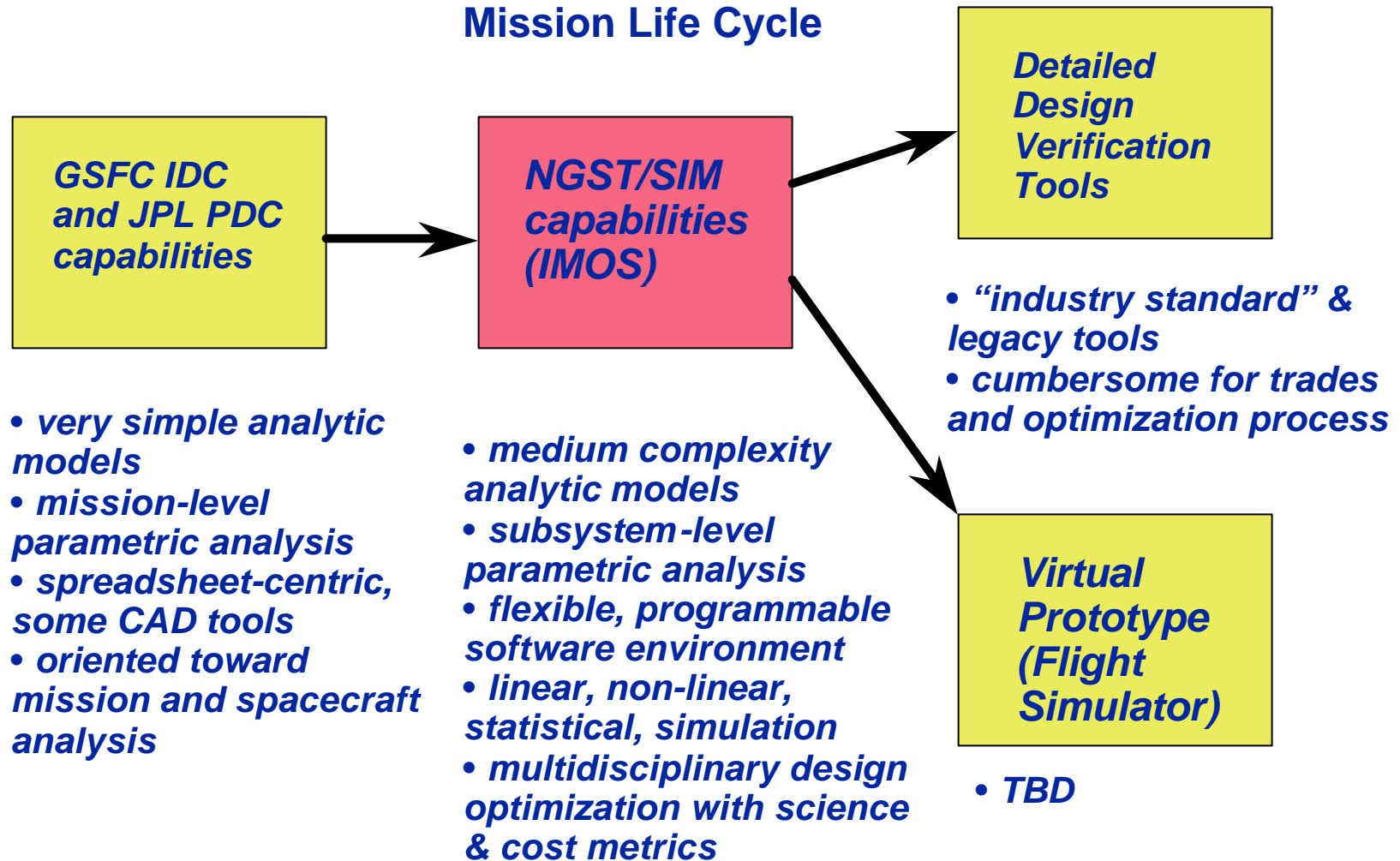
CONCEPTUALIZE

OPTIMIZE/REALIZE

VALIDATE/VERIFY

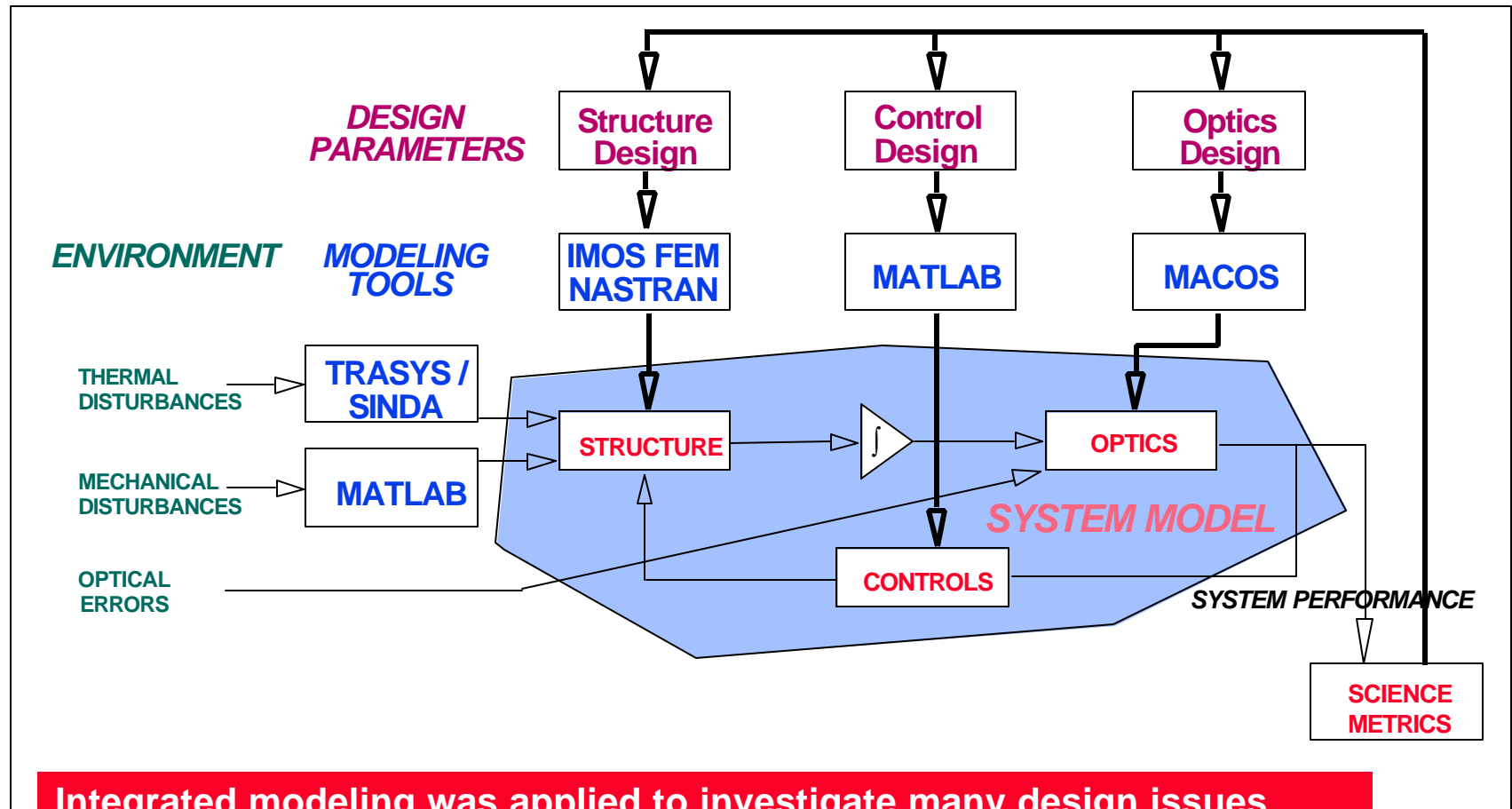


Mission Life Cycle





# IMOS/MACOS Software Environment

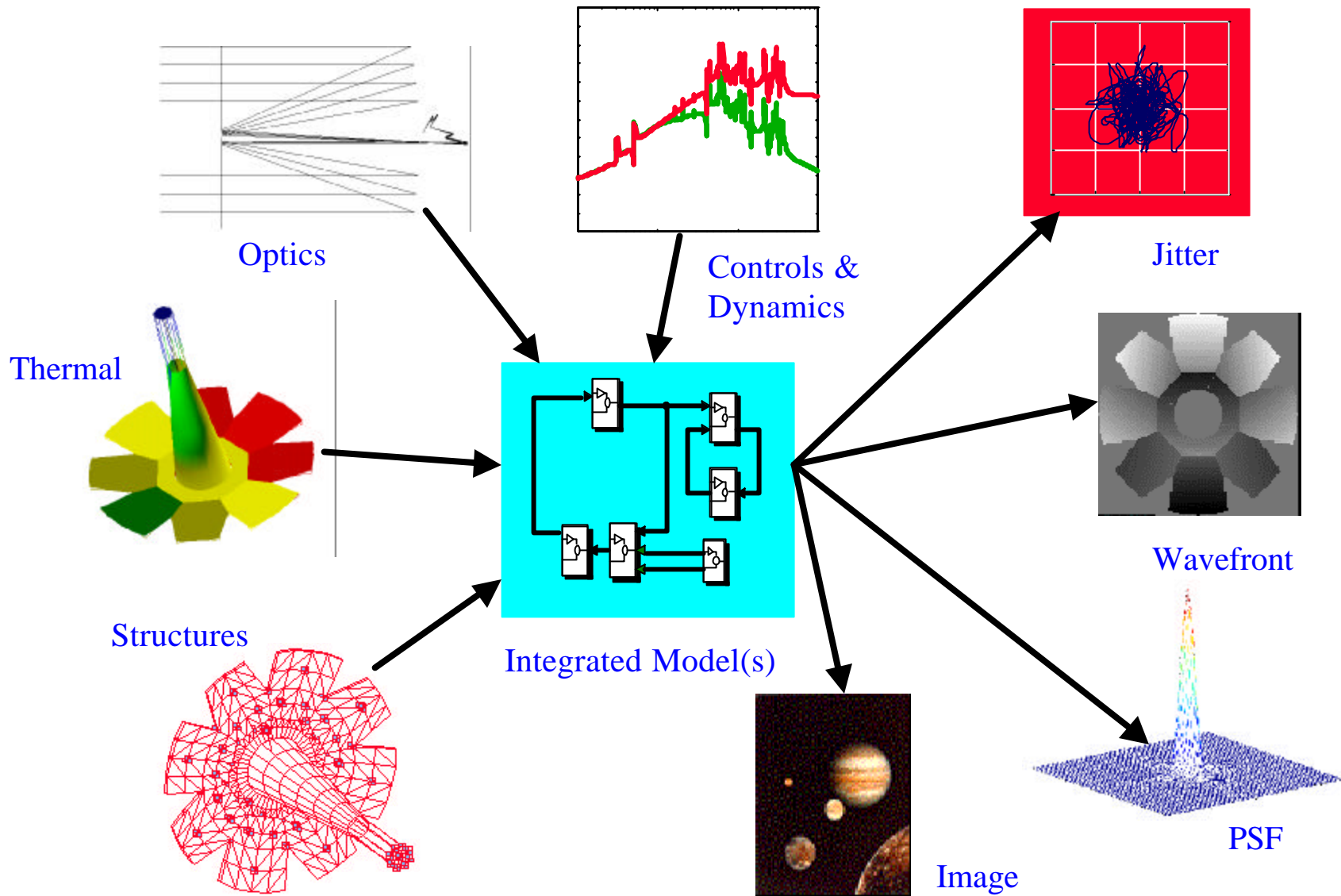


Integrated modeling was applied to investigate many design issues during Phase I studies. Three key problems received the most attention:

- thermal-elastic deformation of OTA (STOP analysis)
- wavefront sensing and control
- line-of-sight stability (jitter)

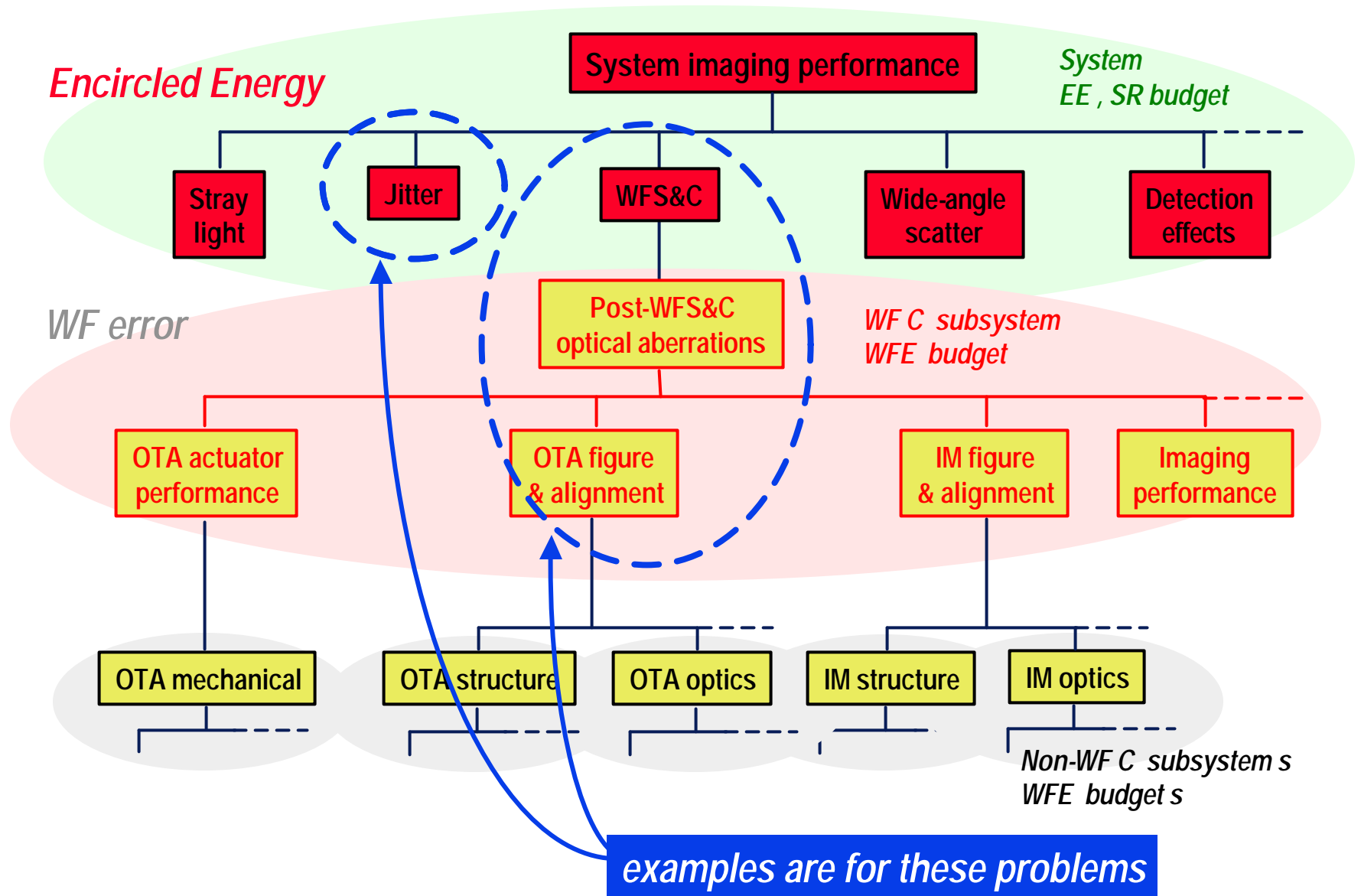


# Key NGST Integrated Analysis Products





# NGST System Error Budgets - Example





# **Design Verification Analysis Example #1**

**“Yardstick” Opto-Mechanical  
Stability (incl. Wavefront Control)**



## Example #1 Problem Statement



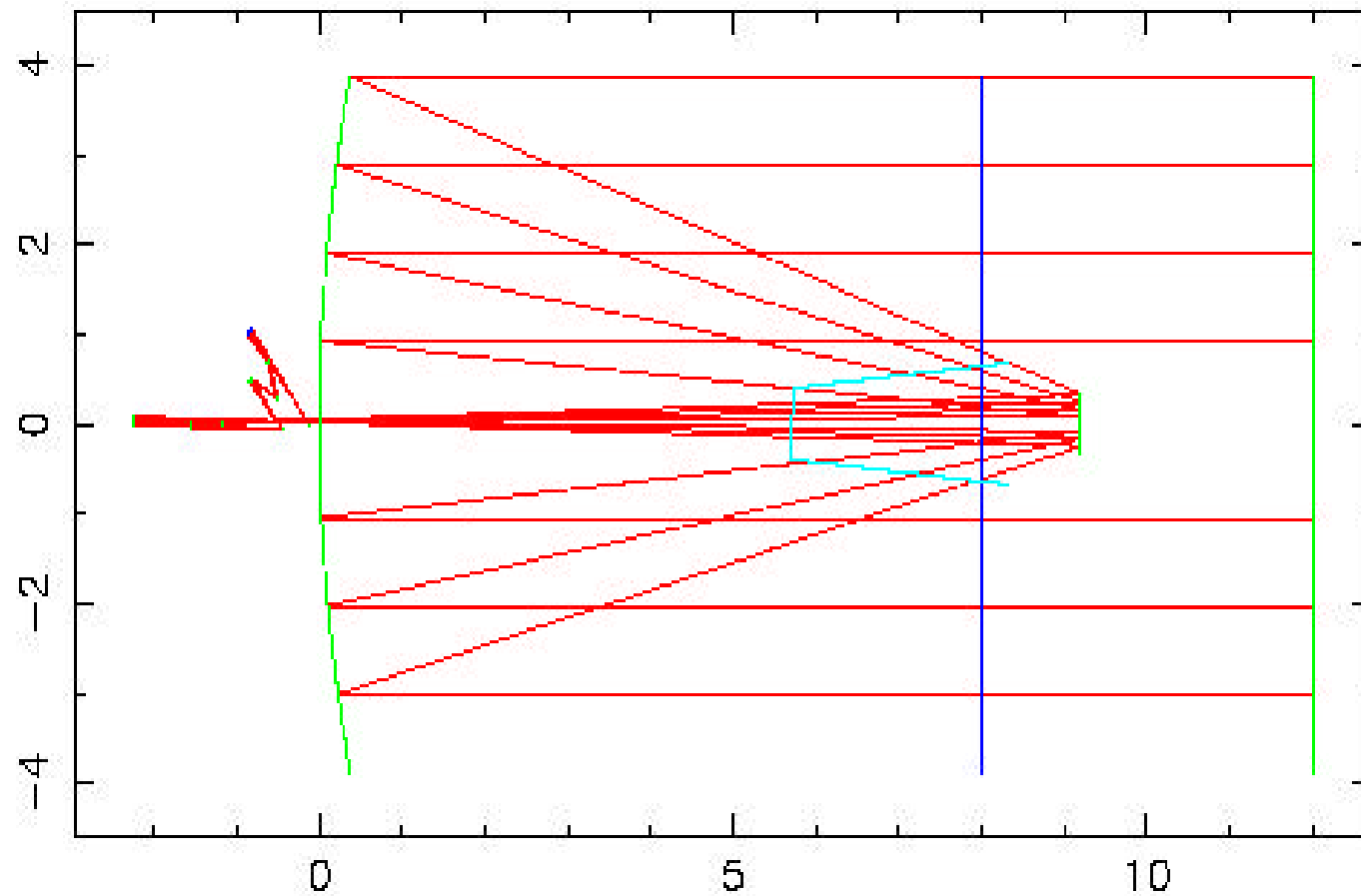
- **Construct a model that simulates the problem of initial alignment and phasing of the optics following launch and deployment.**
  - **Key assumption: only consider thermal-elastic deformation of the Optical Telescope Assembly**
  - **Key assumption: wavefront error sensing is perfect**
  - **Key assumption: wavefront control effected via electro-mechanical actuators (rigid-body on segments plus deformable mirror at pupil)**
  - **Evaluate the performance of the wavefront control system via STOP analysis coupled to active optics simulation**



# Optical Ray Trace Model (MACOS)



Layout, XZ Plane, File=nnf



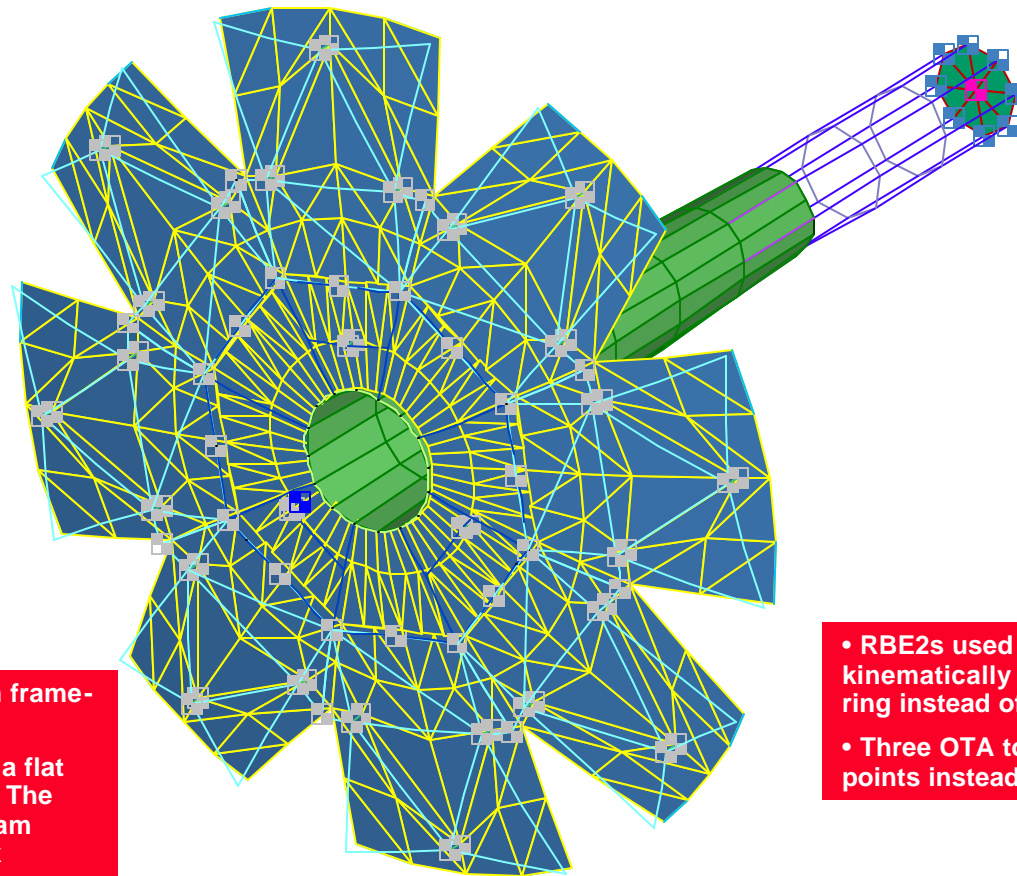


# OTA FEM (IMOS)



- recover 1044 DOFs (344 nodes on PM, translation only, plus SM and SI)

- 2.00mm thick face sheet by 4cm deep core orthogrid beryllium mirror shell
- cells are 14.5 cm on a side equilateral triangles, cell wall are 1.00 mm thick



- The petal reaction structure is a beryllium framework of I-beams
- The center segment reaction structure is a flat Beryllium frame with a 1.3M dia inner ring. The frame is composed of a 152 mm deep I-beam inner ring and 152mm by 100mm wide box section outer ring and spokes.

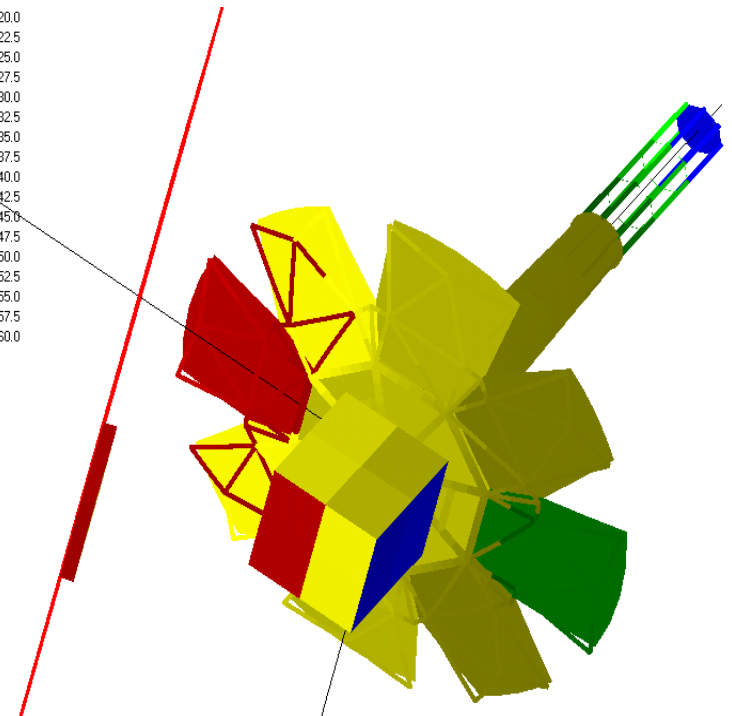
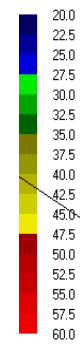
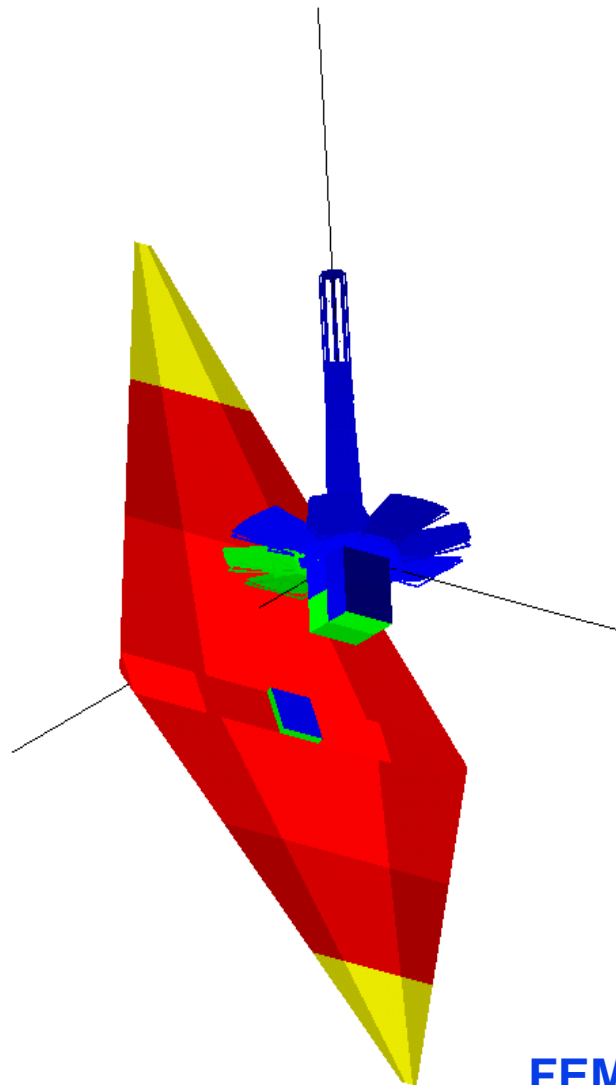
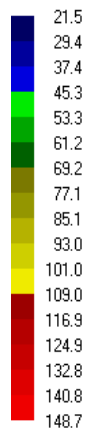
- RBE2s used to attach SI kinematically to center main ring instead of CELAS
- Three OTA to S/C I/F points instead of four

PATRAN → NASTRAN → IMOS





# Observatory Thermal Model (IMOS)



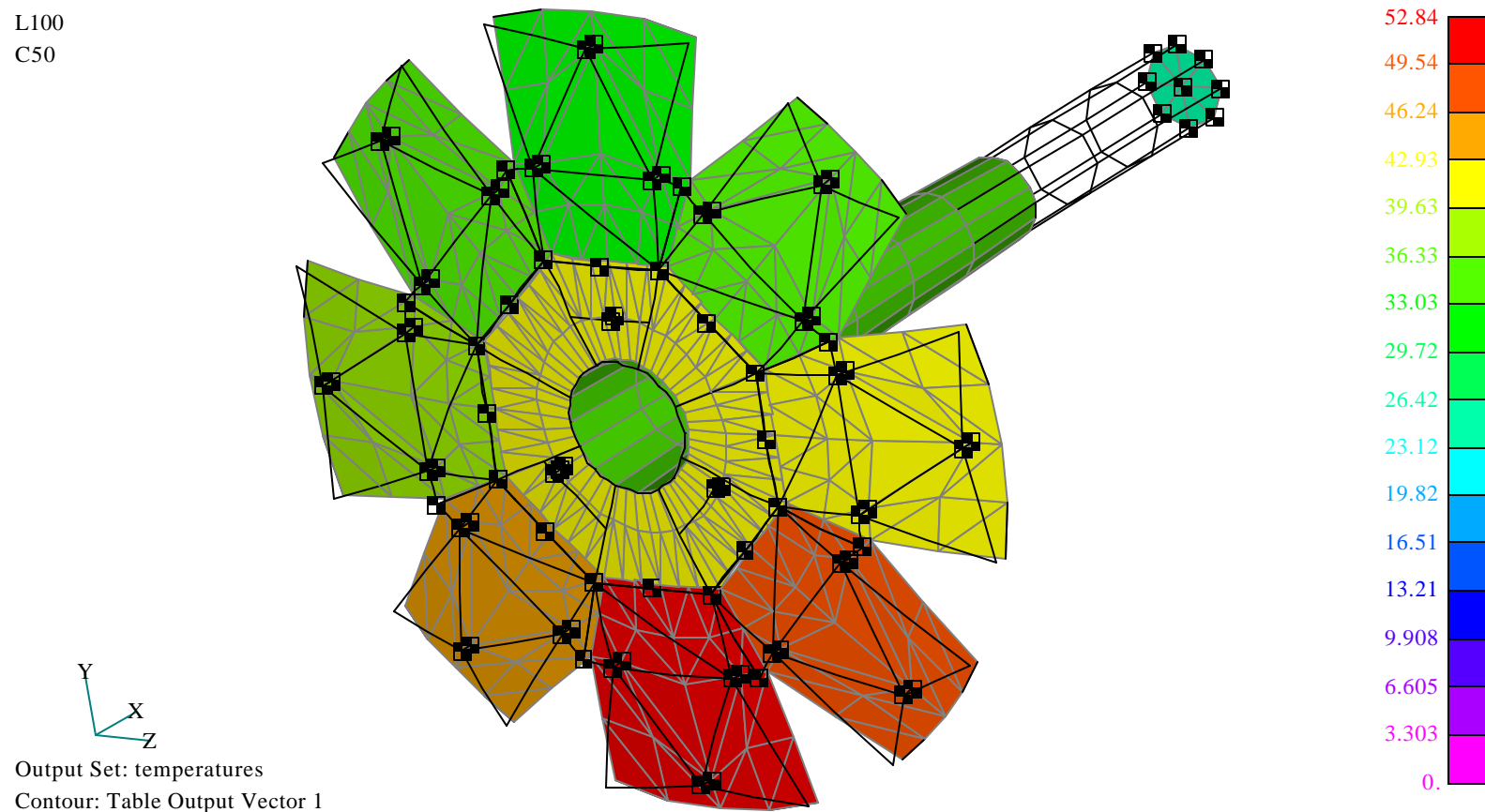
FEMAP → TSS/SINDA → IMOS



# Steady State Temps Mapped on OTA FEM



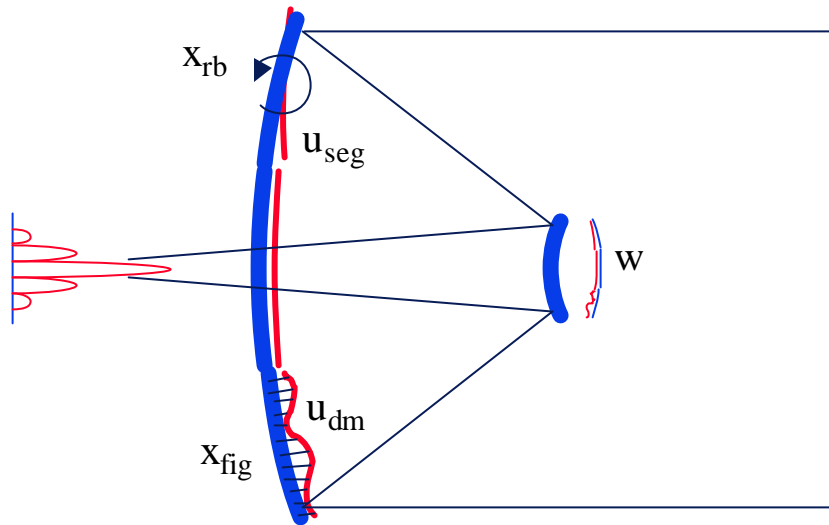
V1  
L100  
C50



**Mapping done by brute-force replication of FEM nodes  
in the thermal conduction model – not best choice**



# Linear Error Model for Wavefront Error Analysis



$$\mathbf{x} = \begin{bmatrix} X_{segrot} \\ X_{segtrans} \\ X_{IMrot} \\ X_{IMtrans} \\ X_{fig} \\ \vdots \end{bmatrix} \quad \text{Alignment and figure states}$$

$$\mathbf{w} = \begin{bmatrix} w_1 \\ w_2 \\ \vdots \\ w_N \end{bmatrix} \quad \text{Wavefront sampled at } N \text{ discrete points in the exit pupil}$$

## Linear optical model

$$\mathbf{w}_0 = \mathbf{C}_x \mathbf{x} + \mathbf{C}_u \mathbf{u}_0$$

## WF sensing

$$\mathbf{w}_{est} = \mathbf{w}_0 + \mathbf{dw}_{est}$$

## Control

$$\mathbf{u}_1 = -\mathbf{G} \mathbf{w}_{est} + \mathbf{du}$$

$$\mathbf{G} = \mathbf{C}_u^+ = [\mathbf{C}_u^T \mathbf{C}_u]^{-1} \mathbf{C}_u$$

**C's are matrices of sensitivity coefficients obtained from perturbation analysis of ray trace model (very difficult to do without MACOS)**

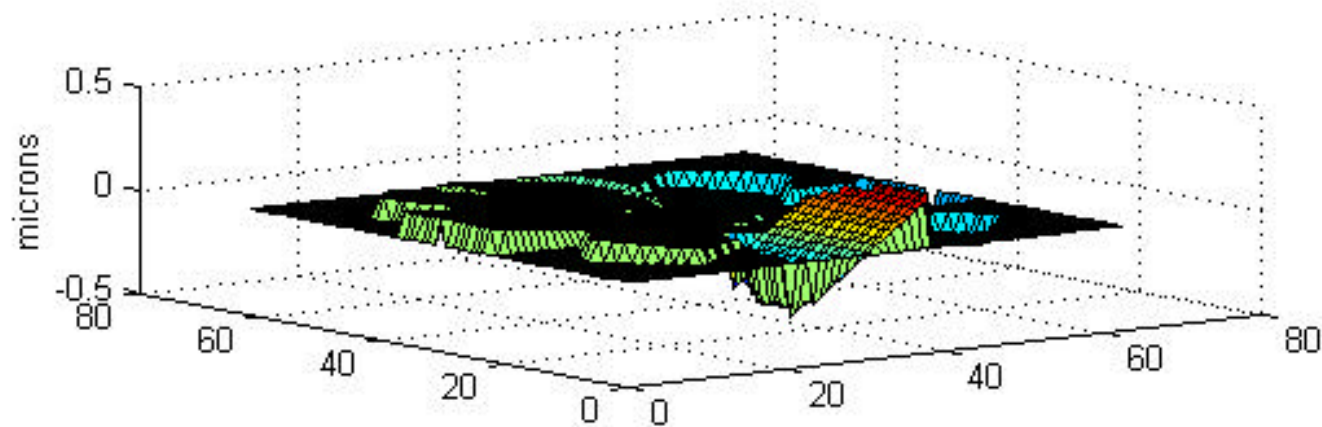
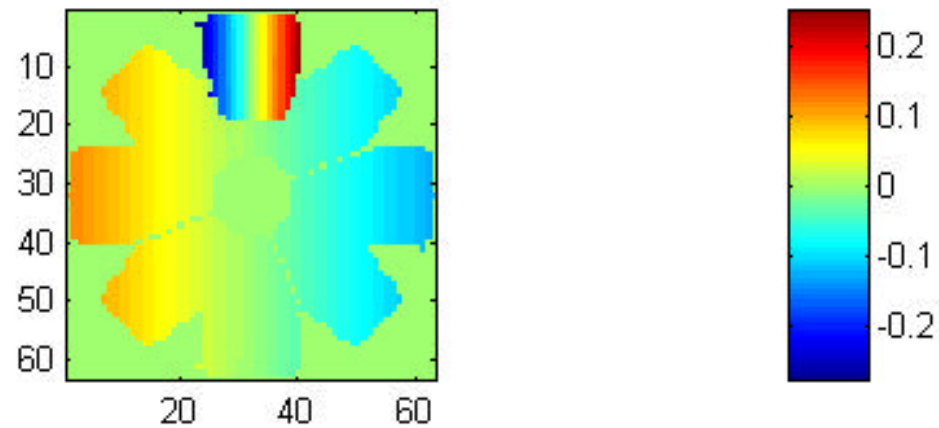
$$\mathbf{u} = \begin{bmatrix} u_{segrot} \\ u_{segtrans} \\ u_{SM} \\ u_{dm} \\ \vdots \end{bmatrix} \quad \text{Optical controls}$$



## Example: Wavefront Error due to Segment Tilt



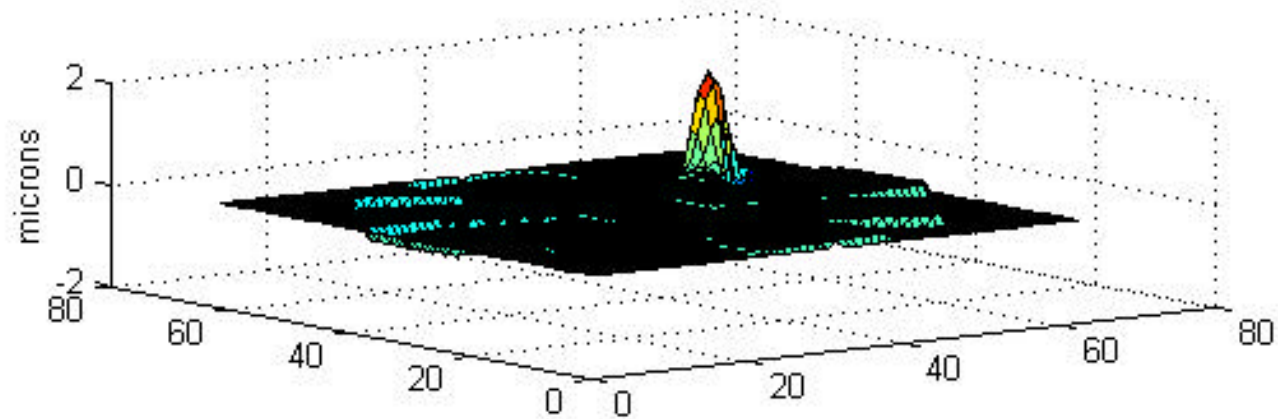
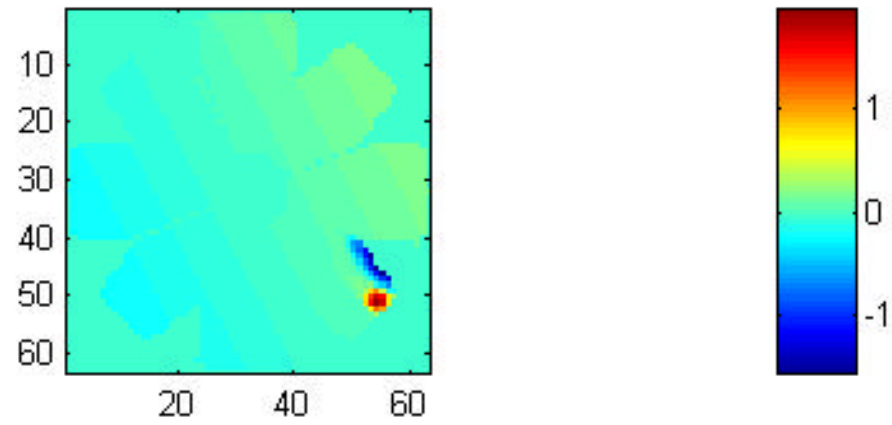
Wavefront Error, 1 urad tilt of segment 5





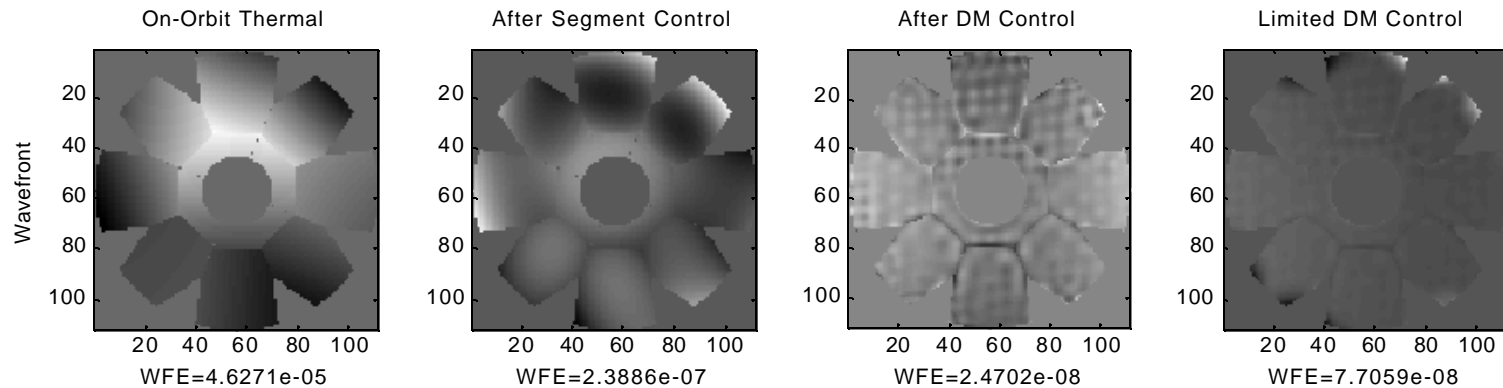
## Example: Wavefront Error due to FEM Node Translation

Wavefront Error, 1 micron X-translation, node 188

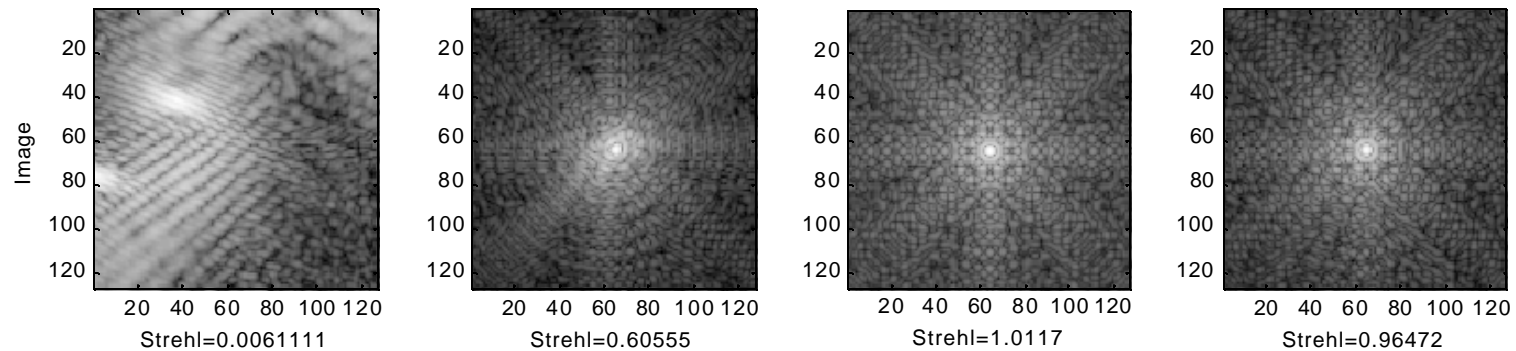




# Wavefront Control applied following Ground-to-Orbit Cooldown



**Temperatures mapped onto structure → deformations mapped into optics → mechanical control corrects optics**





## Comments for Example #1



- **Several integrated environments or utilities based on standards (NASTRAN, SINDA, CODE V, etc.) exist or are coming on line:**
  - IDEAS/TMG
  - FEMAP/TCON
  - Thermal Desktop
  - OptiOpt
  - IODA
- **The above are typical of “glueware”, where data passed between applications “in the pipeline” via files**
- **IMOS/MACOS chosen due to unique capabilities that greatly facilitated the wavefront control simulation – IMOS & MACOS have a programming interface that avoids the “glueware” approach**
- **CODE V, OSLO, ZEMAX now (or will soon) possess similar capability**



# **Design Verification Analysis Example #2**

## **“Yardstick” Line-of-sight Stability**



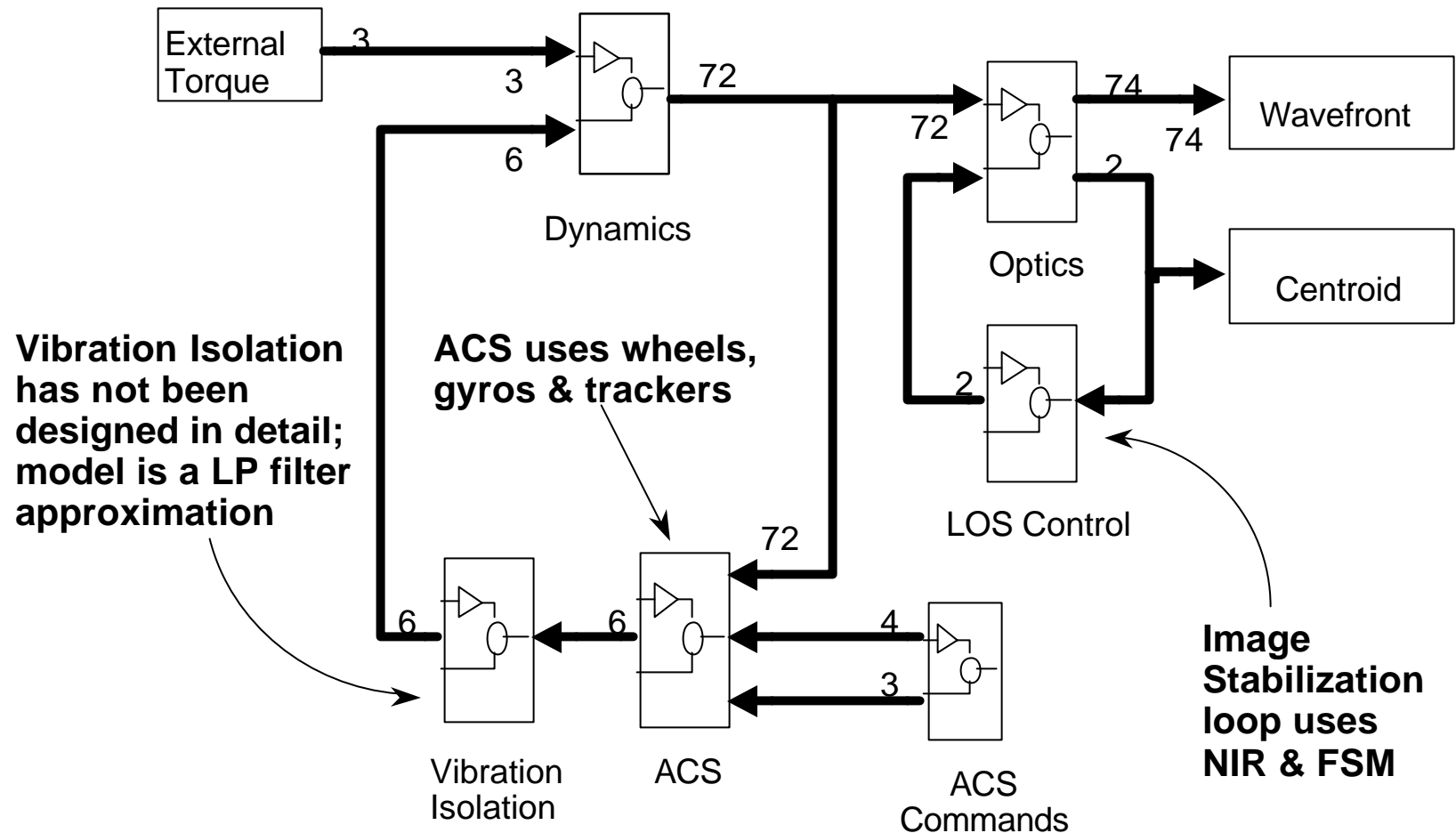


## Example #2 Problem Statement

- **Construct a model that simulates the line-of-sight stability of the system**
  - **Key assumption: only consider errors due to pointing/attitude sensor noise sources and reaction wheel imbalance loads**
  - **Key assumption: dynamic system is linear and time-invariant**
  - **Key assumption: modal damping factor is 0.1%**
  - **Given the top-level line-of-sight error allocation, perform a parametric analysis to determine the requirements for a reaction wheel vibration isolation system**



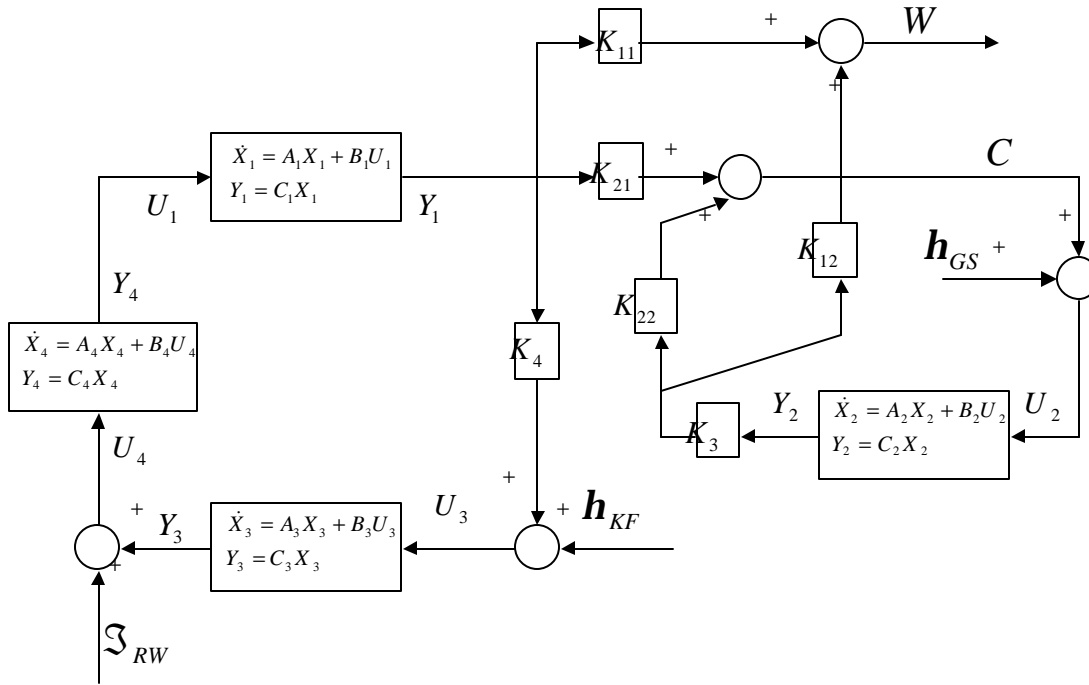
## Pointing Control System Block Diagram



**Simulation equivalent to XTE “Hi-Fi” built using visual modeling tool (Simulink™) in a fraction of the time**



# State-Space Model for Jitter Analysis



$$\dot{X} = AX + BU$$

$$Y = CX$$

$$S_W = \sqrt{\frac{W^T W}{N_{rays}}}$$

$$S_C = \sqrt{C^T C}$$

$$A = \begin{bmatrix} A_1 & 0 & 0 & B_1 C_4 \\ B_2 K_{21} C_1 & A_2 + B_2 K_{22} C_2 & 0 & 0 \\ B_3 K_4 C_1 & 0 & A_3 & 0 \\ 0 & 0 & B_4 C_3 & A_4 \end{bmatrix} \quad X = \begin{bmatrix} X_1 \\ X_2 \\ X_3 \\ X_4 \end{bmatrix} \quad U = \begin{bmatrix} h_{GS} \\ h_{KF} \\ \mathfrak{S}_{RW} \end{bmatrix} \quad Y = \begin{bmatrix} W \\ C \end{bmatrix}$$

$$B = \begin{bmatrix} 0 & 0 & 0 \\ B_2 & 0 & 0 \\ 0 & B_3 & 0 \\ 0 & 0 & B_4 \end{bmatrix} \quad C = \begin{bmatrix} K_{11} C_1 & K_{12} C_2 & 0 & 0 \\ K_{21} C_1 & K_{22} C_2 & 0 & 0 \end{bmatrix}$$

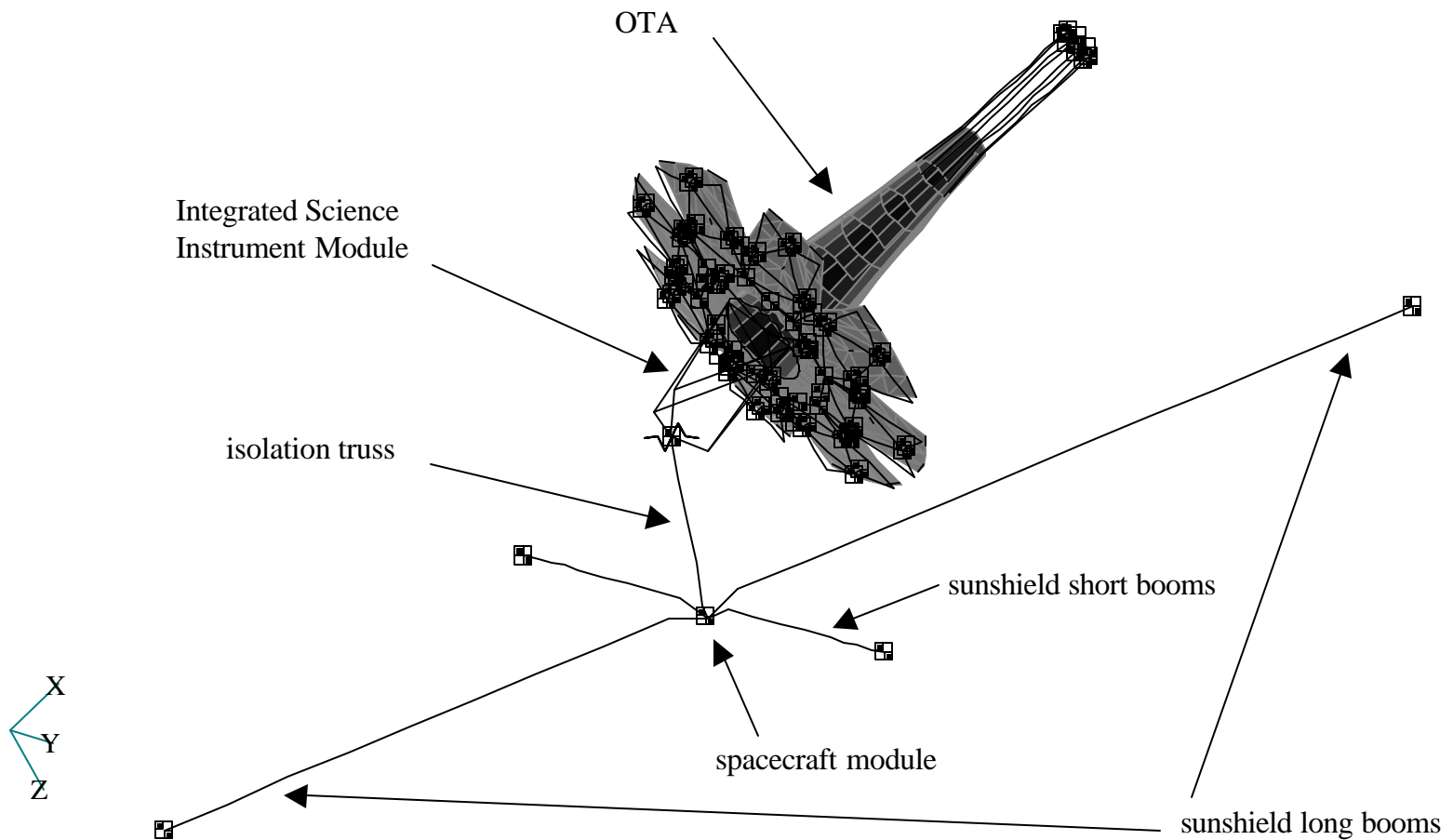
**Developed in parallel with and traceable to the time-domain simulation – the latter was used to verify results from the linear analysis**



# Observatory FEM (IMOS)

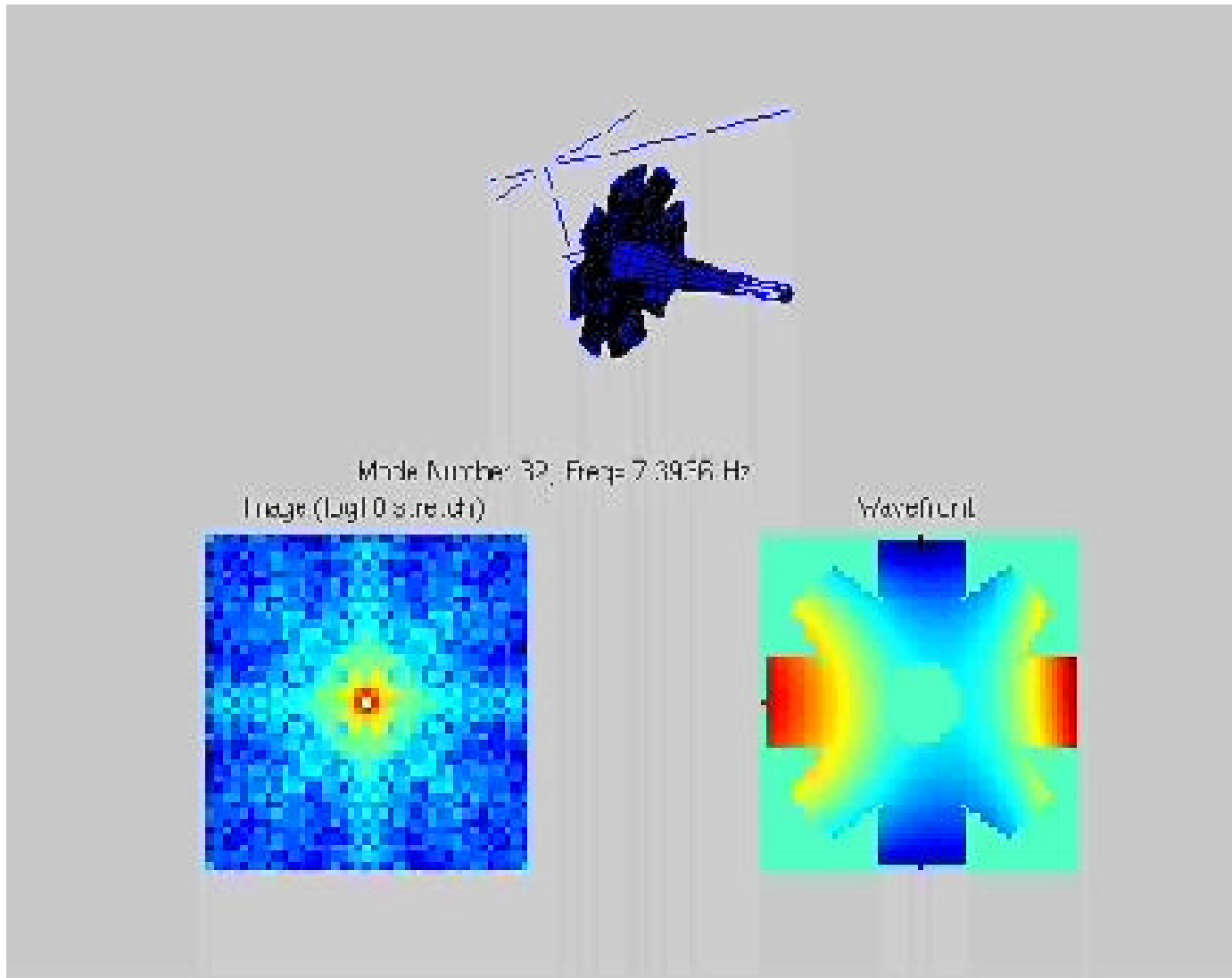


**Model contains ~5400 DOF, low- to -medium fidelity**





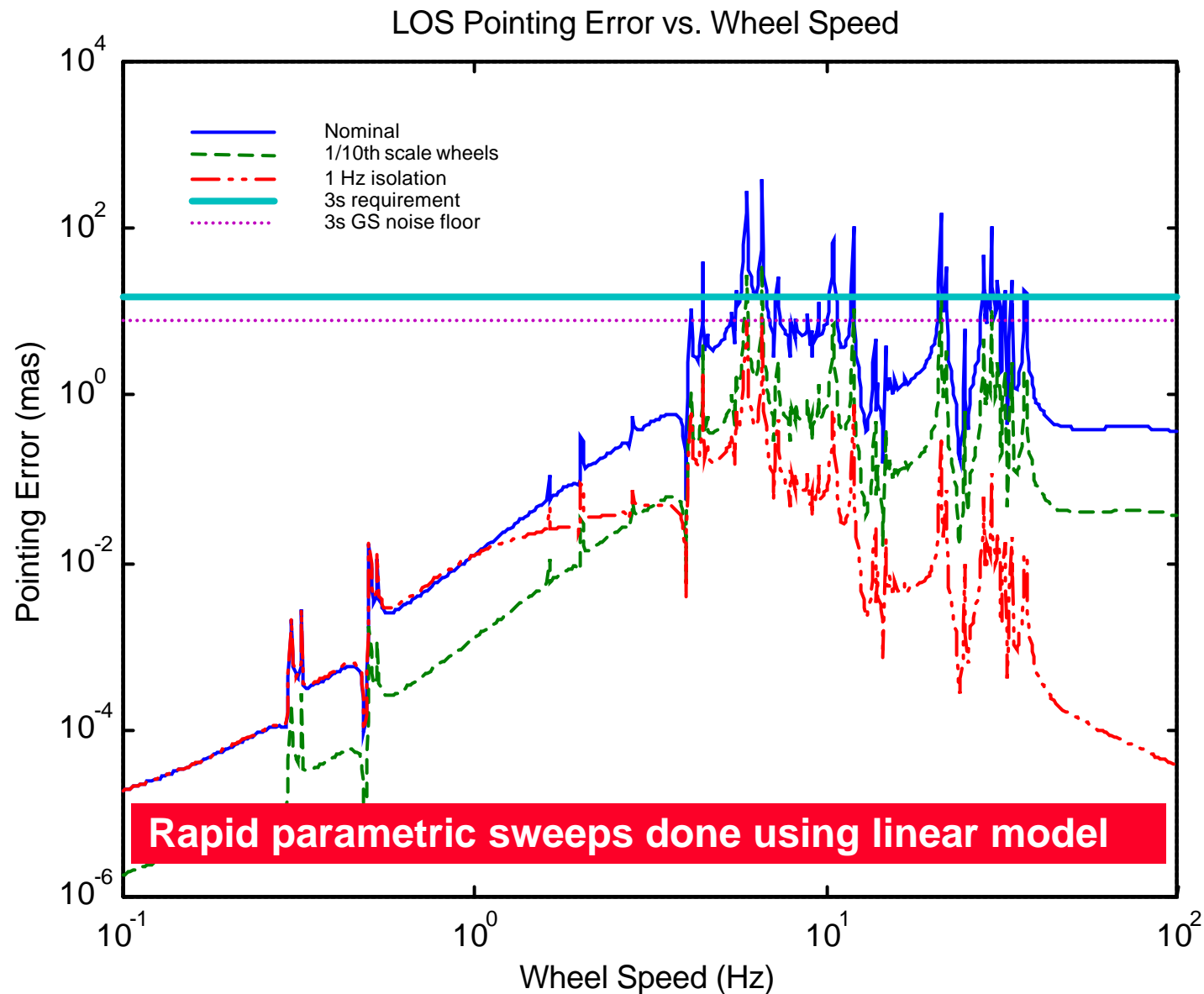
# Opto-Mechanical Analysis



***Structural dynamics (mode shapes) and equivalent aberrations are animated – visualization helpful to modeling team***

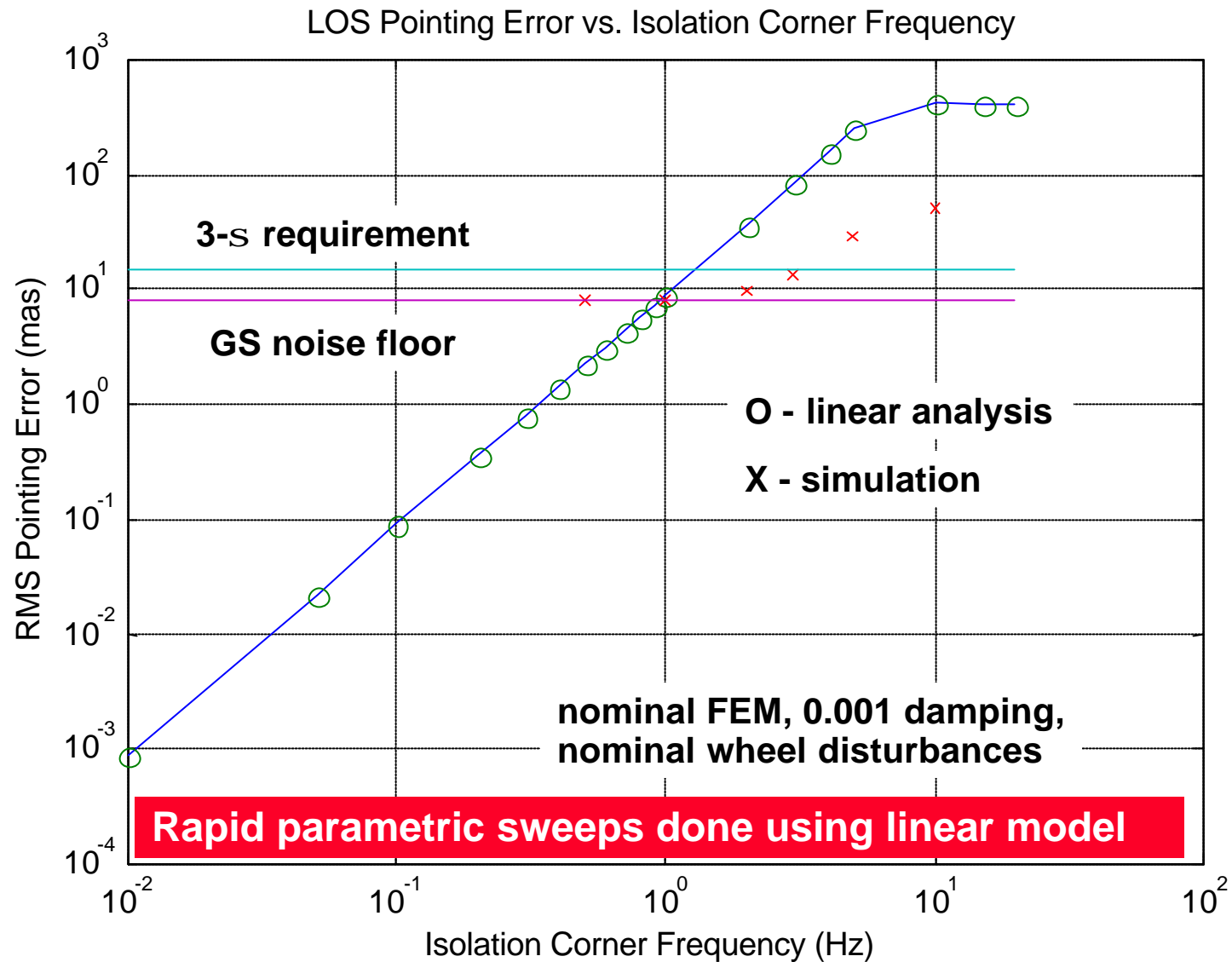


# Linear Analysis - Nominal Response, Effect of Isolation, Effect of Wheel Imbalance Magnitude





# How Much Isolation Is Required?





# **Sensitivity and ‘Iso-performance’ Example**

## **Nexus Flight Experiment**





## Example #3 Problem Statement



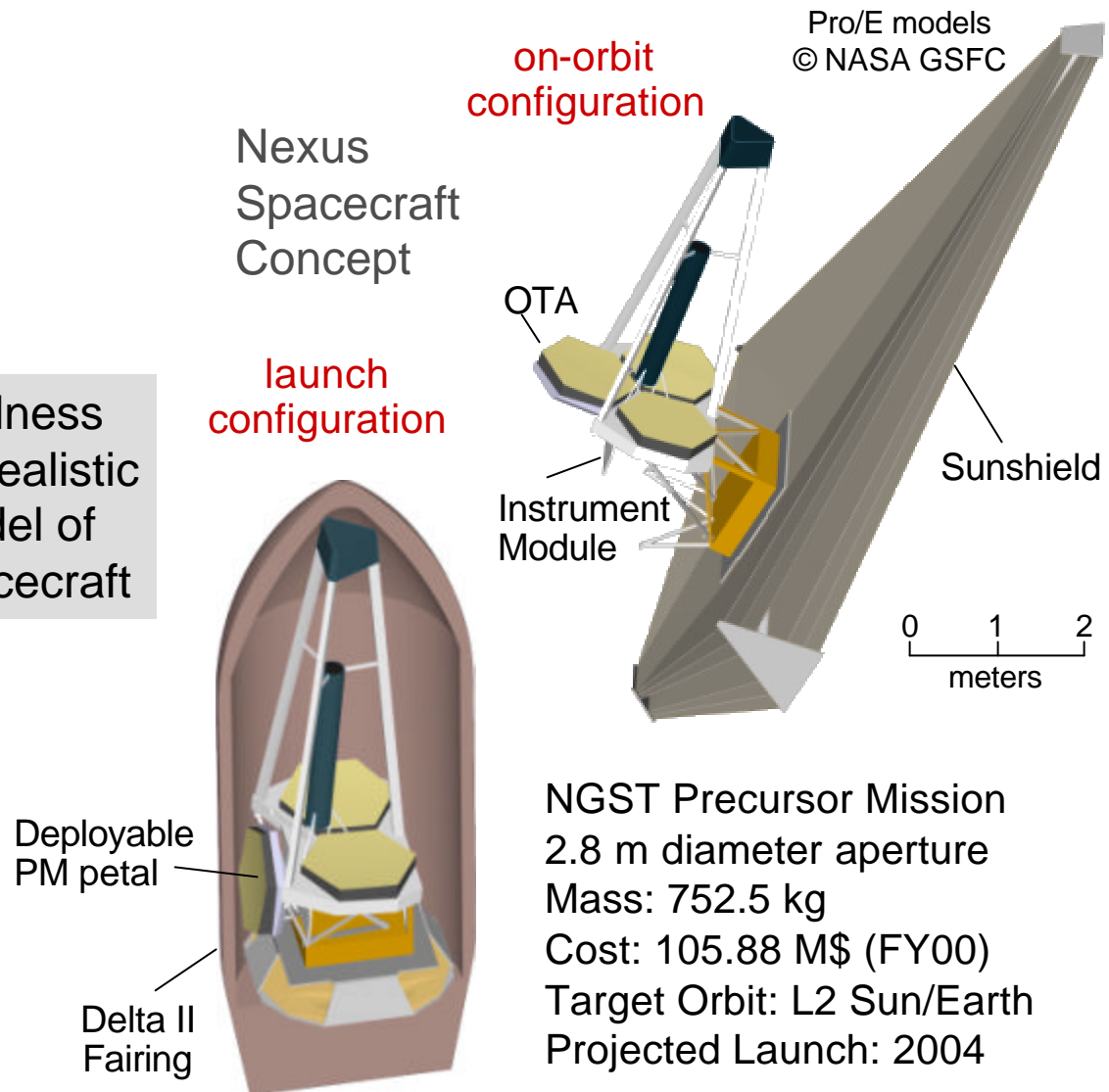
- **Essentially identical to previous example (line-of-sight stability problem)**
- **Exploit techniques recently developed at MIT in order to:**
  - **Compute key design sensitivities (changes in performance metrics as functions of changes in design parameters)**
  - **Enable intelligent design trades by identifying “iso-performance” contours in a multivariate design trade space**



# Nexus Case Study @ MIT

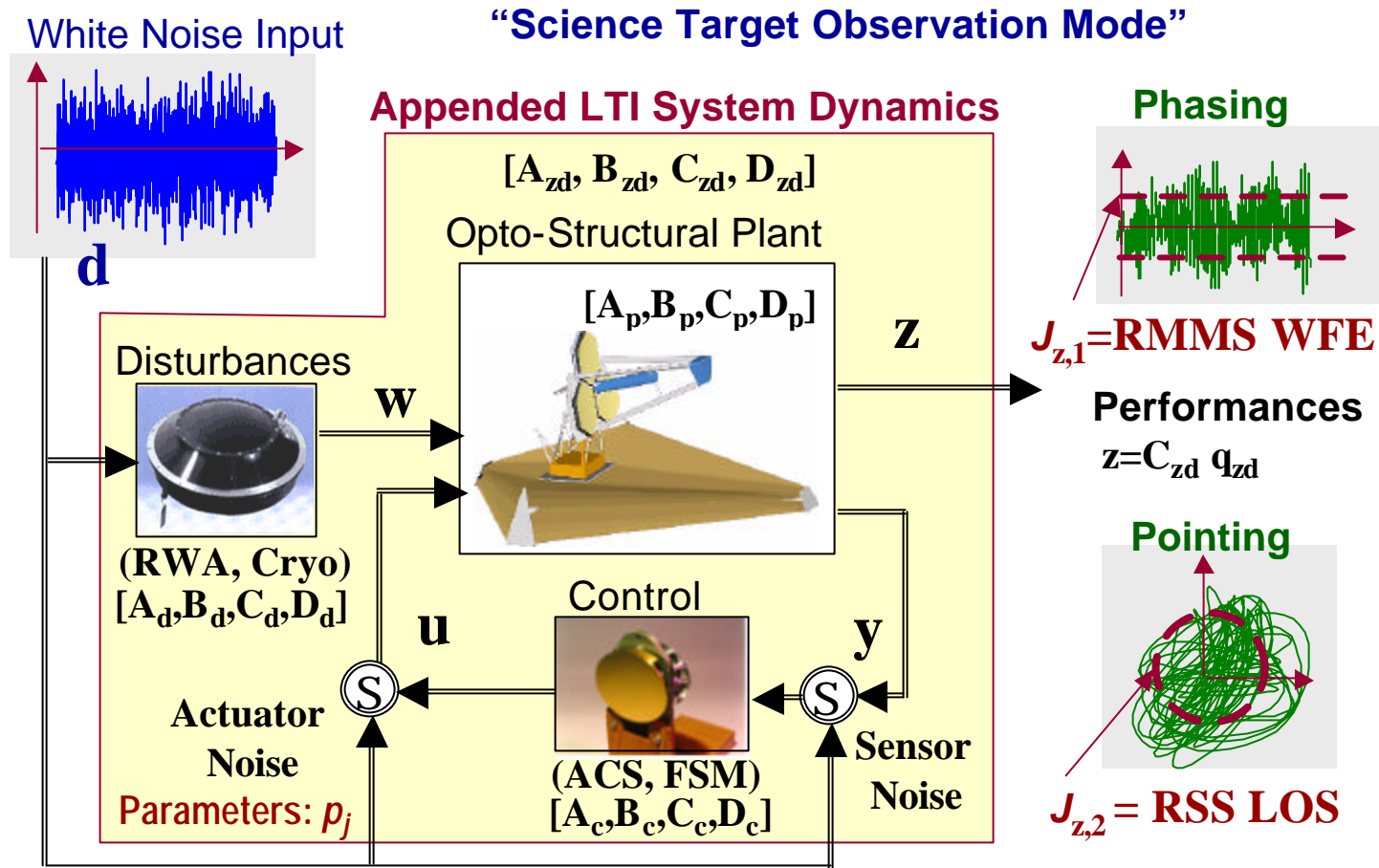


Demonstrate the usefulness of Isoperformance on a realistic conceptual design model of a high-performance spacecraft





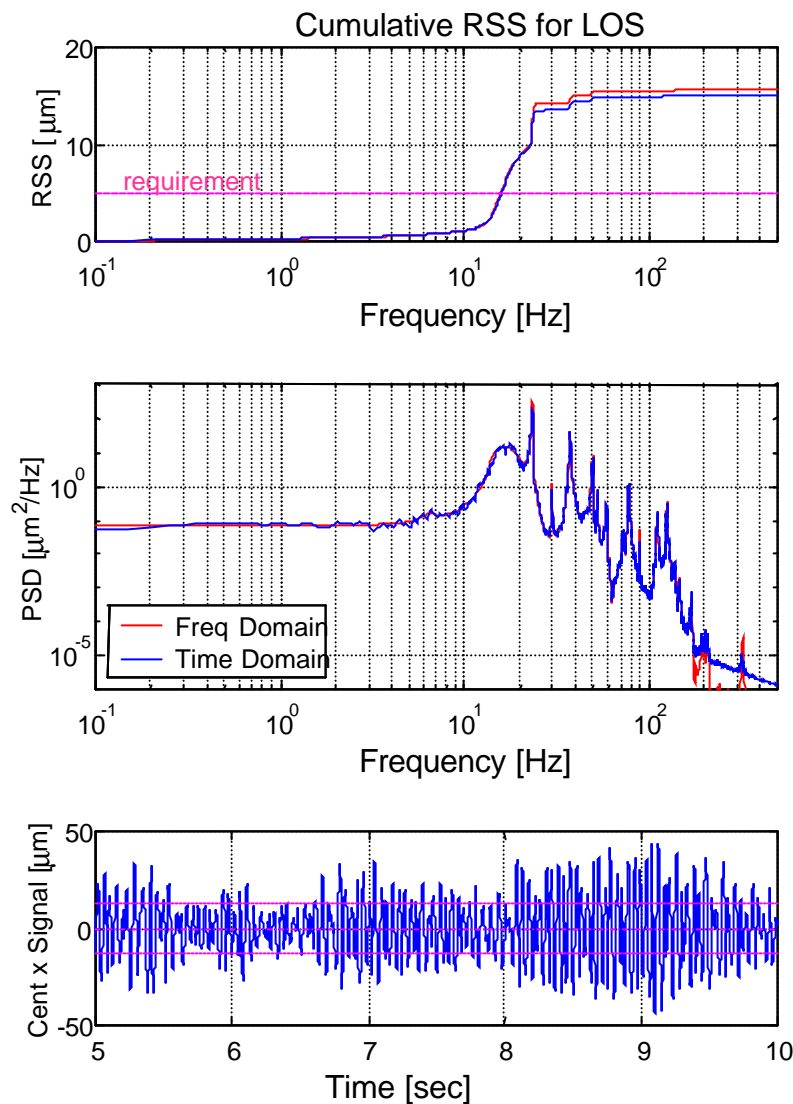
# Problem Setting



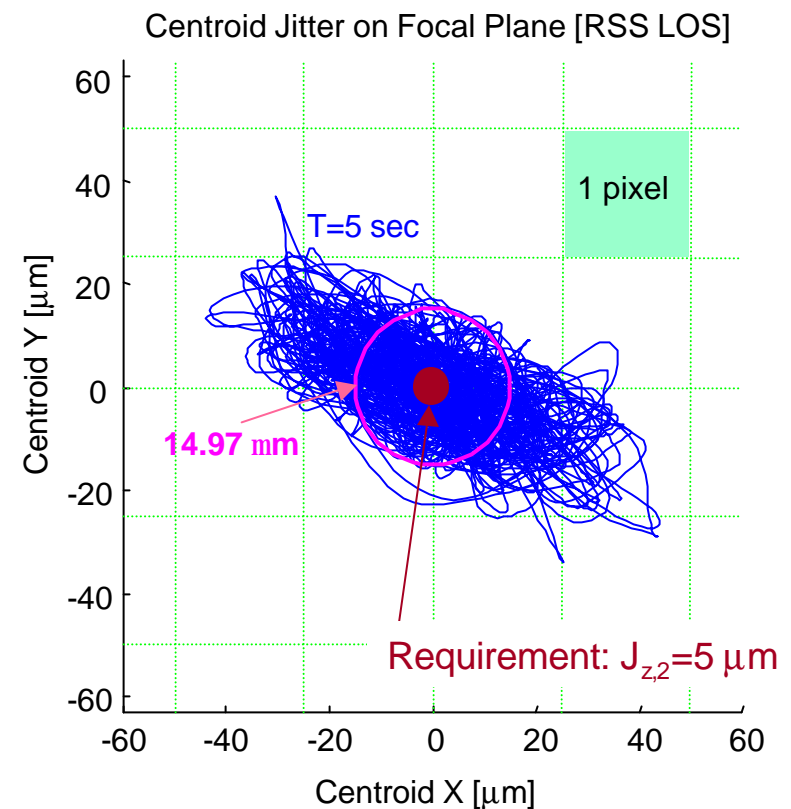
Traditionally: Define System Parameters  $p_j = p_o \longrightarrow$  Predict  $H_2$  performances  $J_{z,i}$   
 Isoperformance: Find Locus of Solutions  $p_{LB} < p_j < p_{UB} \longleftarrow$  Constrain performances  $J_{z,i} = J_{z,req}$



# Initial Performance Assessment $J_z(p^0)$

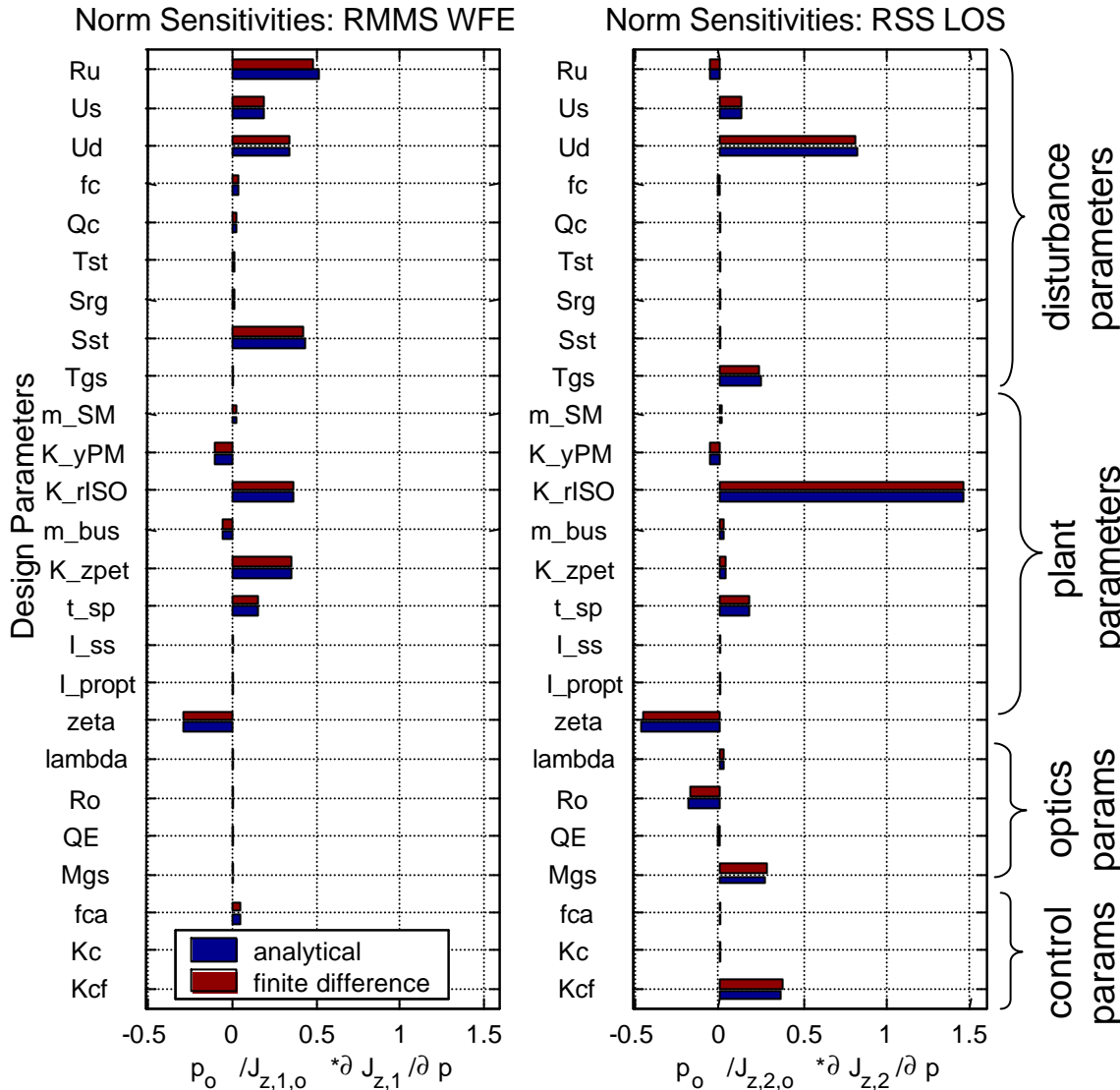


	Results	Lyap/Freq	Time	
$J_{z,1}$ (RMMS WFE)		<b>25.61</b>	<b>19.51</b>	[nm]
$J_{z,2}$ (RSS LOS)		<b>15.51</b>	<b>14.97</b>	[ $\mu\text{m}$ ]





# Nexus Sensitivity Analysis



Graphical Representation of Jacobian evaluated at design  $p_o$ , normalized for comparison.

$$\bar{\nabla} J_z = \frac{p_o}{J_{z,o}} \begin{bmatrix} \frac{\partial J_{z,1}}{\partial R_u} & \frac{\partial J_{z,2}}{\partial R_u} \\ \dots & \dots \\ \frac{\partial J_{z,1}}{\partial K_{cf}} & \frac{\partial J_{z,2}}{\partial K_{cf}} \end{bmatrix}$$

## RMMS WFE most sensitive to:

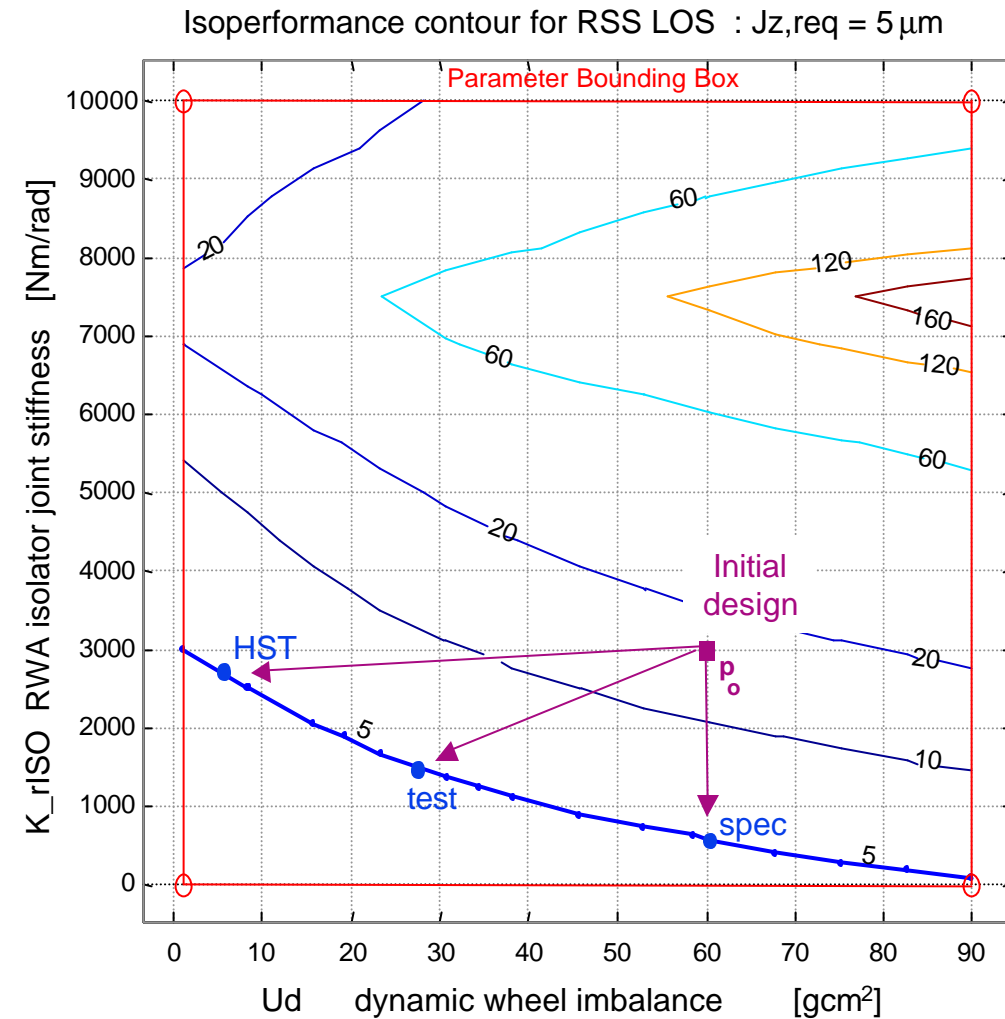
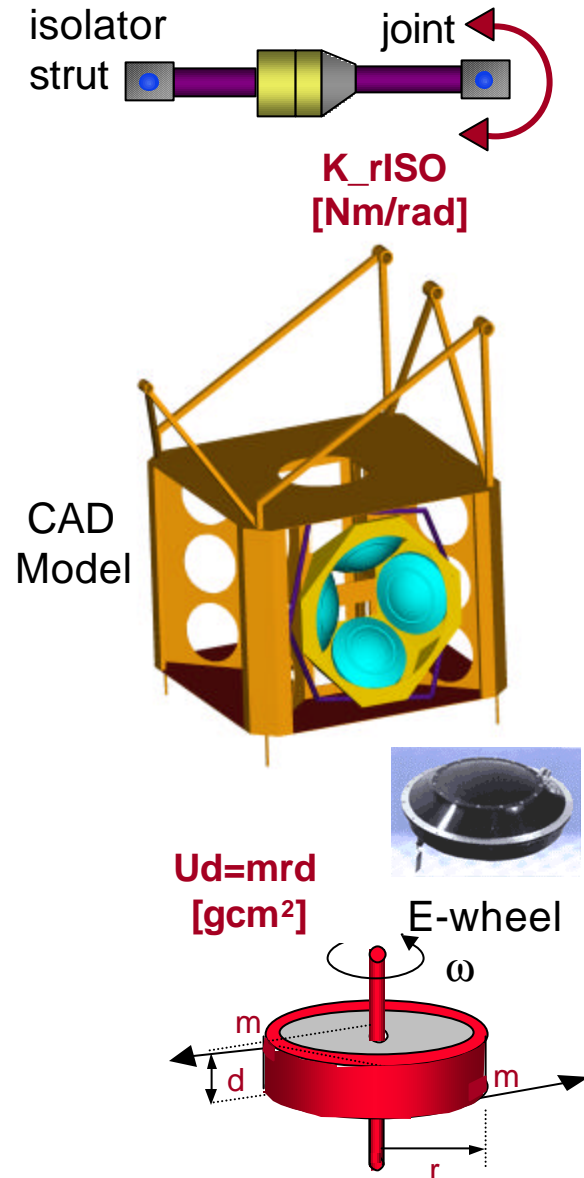
Ru - upper op wheel speed [RPM]  
 Sst - star track noise  $1\sigma$  [asec]  
 K\_rISO - isolator joint stiffness [Nm/rad]  
 K\_zpet - deploy petal stiffness [N/m]

## RSS LOS most sensitive to:

Ud - dynamic wheel imbalance [gcm<sup>2</sup>]  
 K\_rISO - isolator joint stiffness [Nm/rad]  
 zeta - proportional damping ratio [-]  
 Mgs - guide star magnitude [mag]  
 Kcf - FSM controller gain [-]



# 2D-Isoperformance Analysis

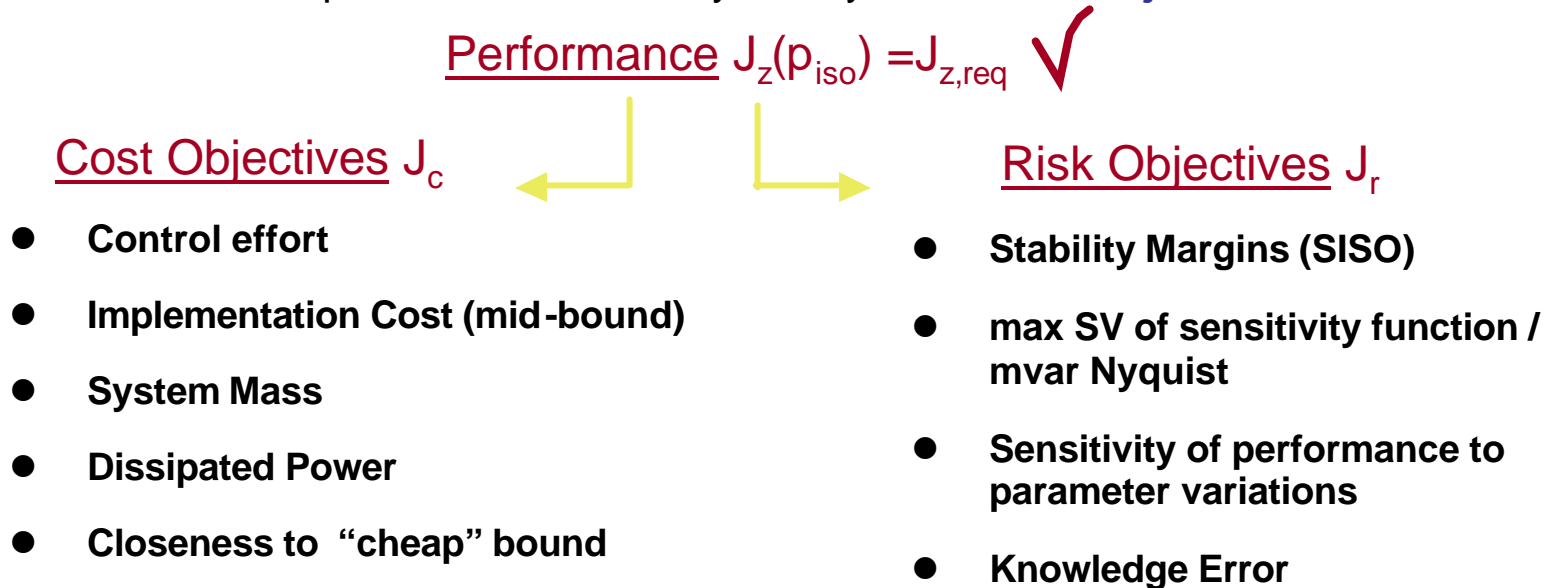




# Multiobjective Design Optimization



Since solutions  $\mathbf{p}_{iso}$  in the isoperformance set  $\mathbf{I}$  do not distinguish themselves via their performance, we may satisfy **additional objectives**:





# Nexus Multivariable Isoperformance $n_p=10$

## Pareto-Optimal Designs $p^*_{iso}$

### Design A

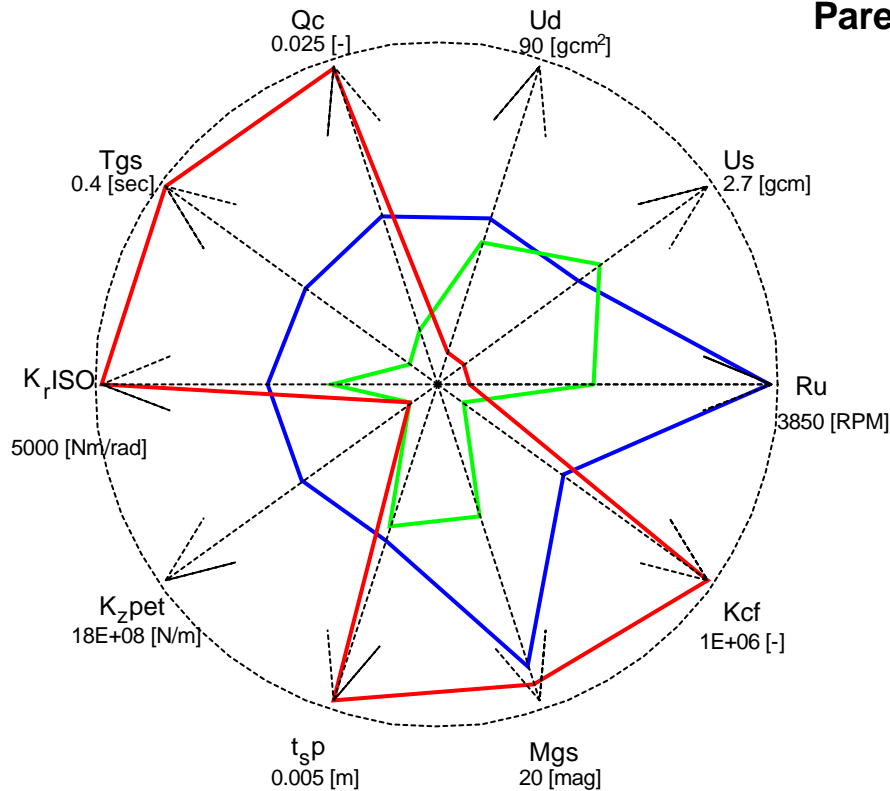
Best “mid-range”  
compromise

### Design B

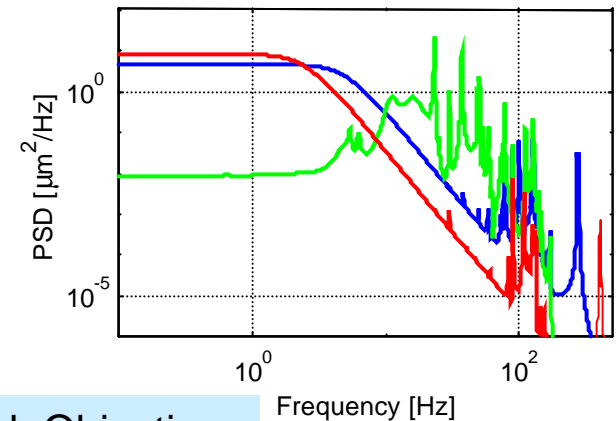
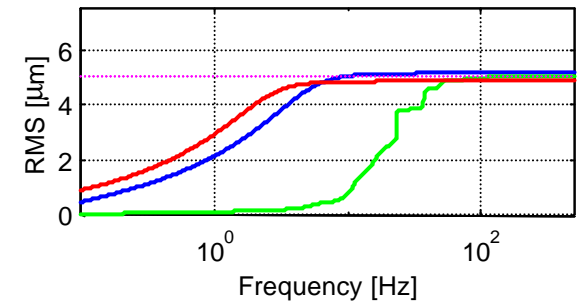
Smallest FSM  
control gain

### Design C

Smallest  
performance  
uncertainty



Cumulative RSS for LOS



## Performance

## Cost and Risk Objectives

— A: $\min(J_{c1})$
— B: $\min(J_{c2})$
— C: $\min(J_{r1})$

Design A

Design B

Design C

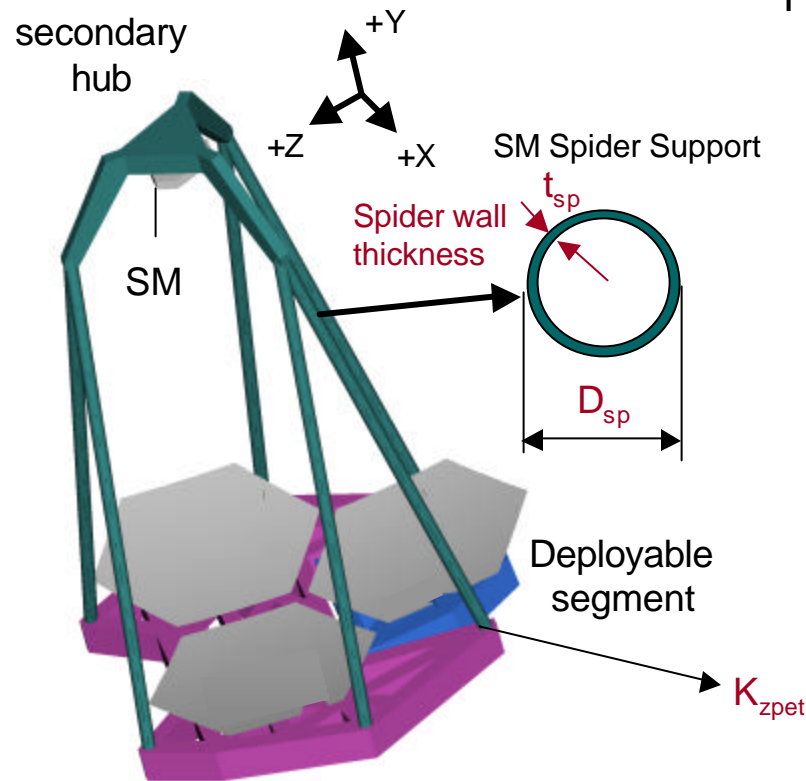
	Jz,1	Jz,2
Design A	20.0000	5.2013
Design B	20.0012	5.0253
Design C	20.0001	4.8559

	Jc,1	Jc,2	Jr,1
Design A	0.6324	0.4668	+/- 14.3218 %
Design B	0.8960	0.0017	+/- 8.7883 %
Design C	1.5627	1.0000	+/- 5.3067 %



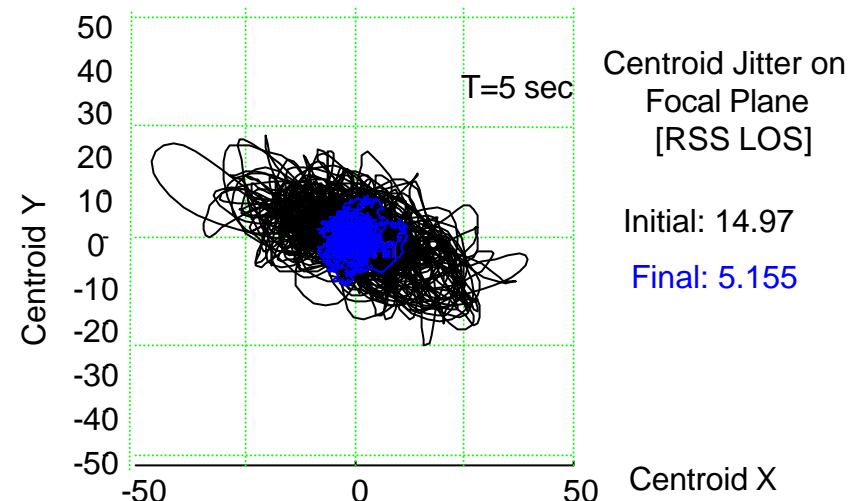


# Nexus Initial $p^0$ vs. Final Design $p^{**}_{iso}$



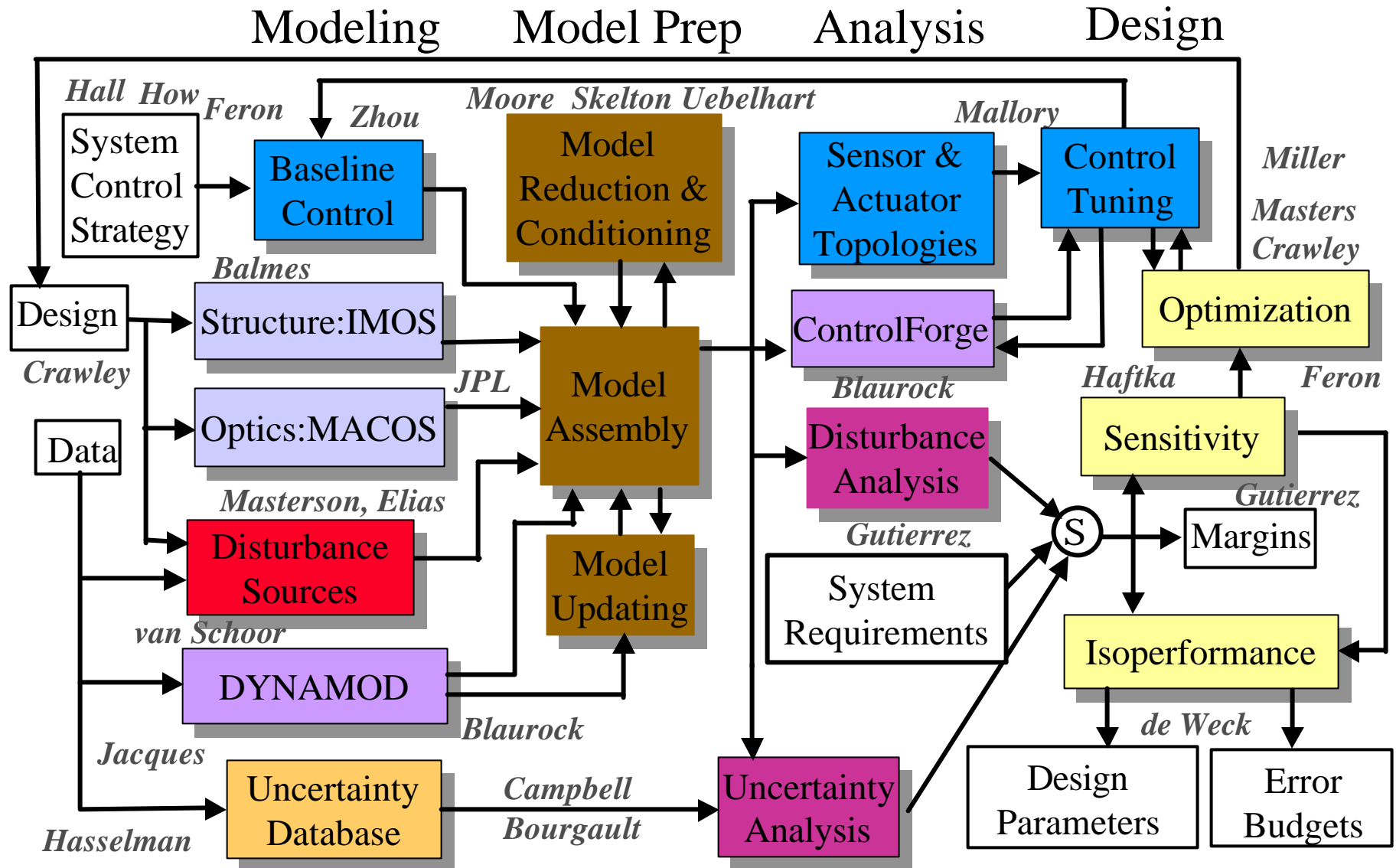
Improvements are achieved by a well balanced mix of changes in the disturbance parameters, structural redesign and increase in control gain of the FSM fine pointing loop.

Parameters	Initial	Final	
$R_u$	3000	3845	[RPM]
$U_s$	1.8	1.45	[gcm]
$U_d$	60	47.2	[gcm <sup>2</sup> ]
$Q_c$	0.005	0.014	[-]
$T_{gs}$	0.040	0.196	[sec]
$K_{rISO}$	3000	2546	[Nm/rad]
$K_{zpet}$	0.9E+8	8.9E+8	[N/m]
$t_{sp}$	0.003	0.003	[m]
$M_{gs}$	15	18.6	[Mag]
$K_{cf}$	2E+3	4.7E+5	[-]





# MIT – DOCS Framework



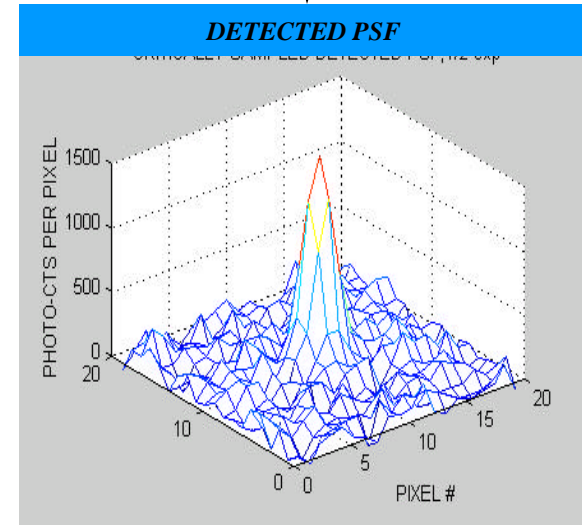
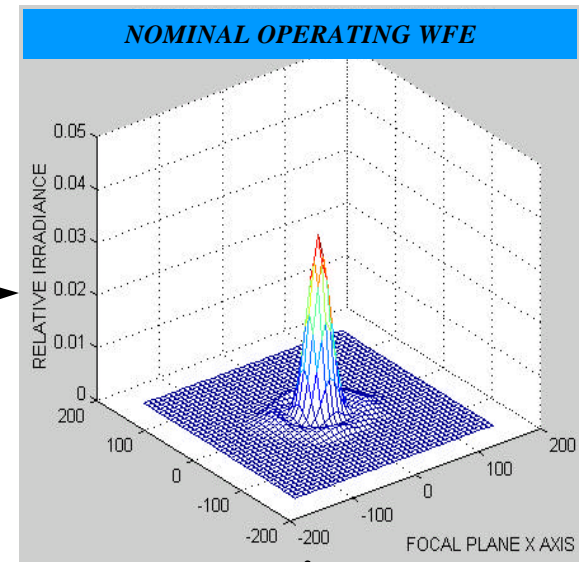
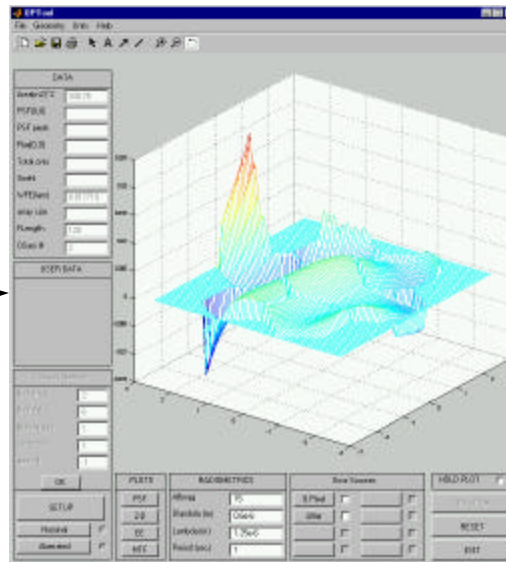
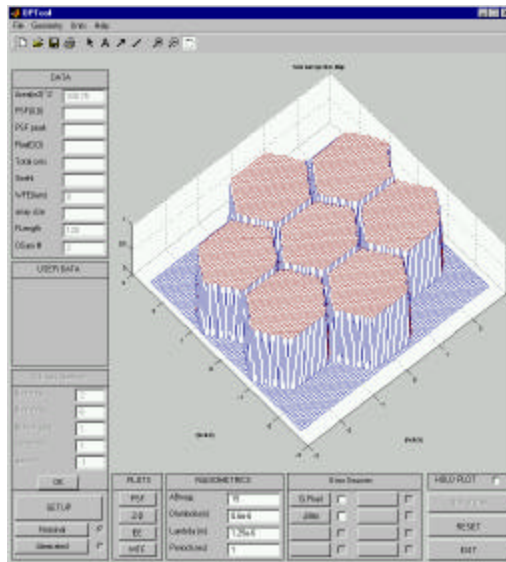


# Requirements Analysis Examples

- **Sensitivity (SNR) Analysis**
- **Wavefront Error Budget Partitioning**



# Sensitivity Analysis via Fourier Optics Modeling



APERTURE GEOMETRY  
PUPIL PHASE ERROR  
JITTER  
STAR MAGNITUDE  
OPTICS THROUGHPUT  
DETECTOR QUANTUM EFFICIENCY  
DETECTOR DARK CURRENT  
STRAY LIGHT & THERMAL EMISSION  
ZODIACAL BACKGROUND  
READ-OUT NOISE  
FLAT FIELD ERRORS  
A/D CONVERSION



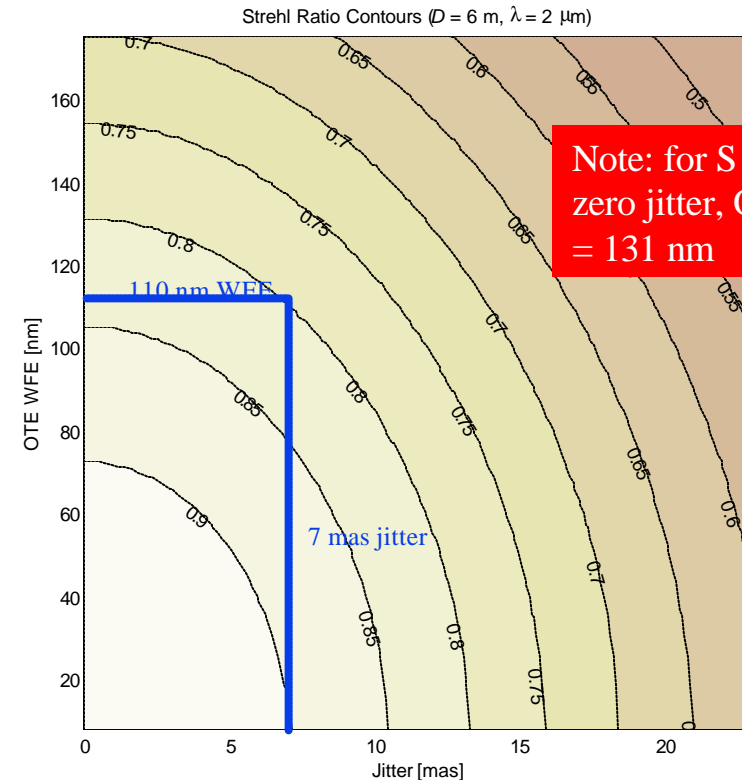
# Wavefront Error Allocation Analysis



A simple derivation  
of the equivalency of  
jitter and RMS  
wavefront error...

$$S = e^{-\left(\frac{2ps_w}{l}\right)^2}$$
$$= \frac{1}{1 + (2.22 s_j D / l)^2}$$

$$s_{w'} = \frac{l}{2p} \sqrt{\ln \left[ 1 + (2.22 s_j D / l)^2 \right]}$$



... leading to a model that  
provides contours of  
constant Strehl ratio as  
functions of jitter and  
“static” wavefront error



## Examples Summary



- From #1 → #5, complexity decreased: measured by model size ( $N_{\text{DOF}}$ ), CPU/Memory load, and software development effort.
- From #1 → #3, number of free variables in model increased, and accordingly, so did the amount of “pre-work” (formulation of problem, solving of equations by hand before code was written, etc.).
- Examples #2 & #3 illustrate the use of “complementary” models – in these cases time-domain simulations used to cross-check results obtained using linear state-space models. The models in examples #4 & #5 are also complimentary.
- Examples #4 & #5, while being the simplest of these examples, are in a real sense the most powerful of all of these analyses, reason being that without good requirements, the rest of the “game” is pointless.
- **WE (the “community”, not just NGST)** are typically better equipped in terms of tools, skills, and experience at solving problems such as #1 and #2 than any of the others.



## **Other Lessons Learned in NGST Phase I**



## A Broader Perspective for Integrated Modeling

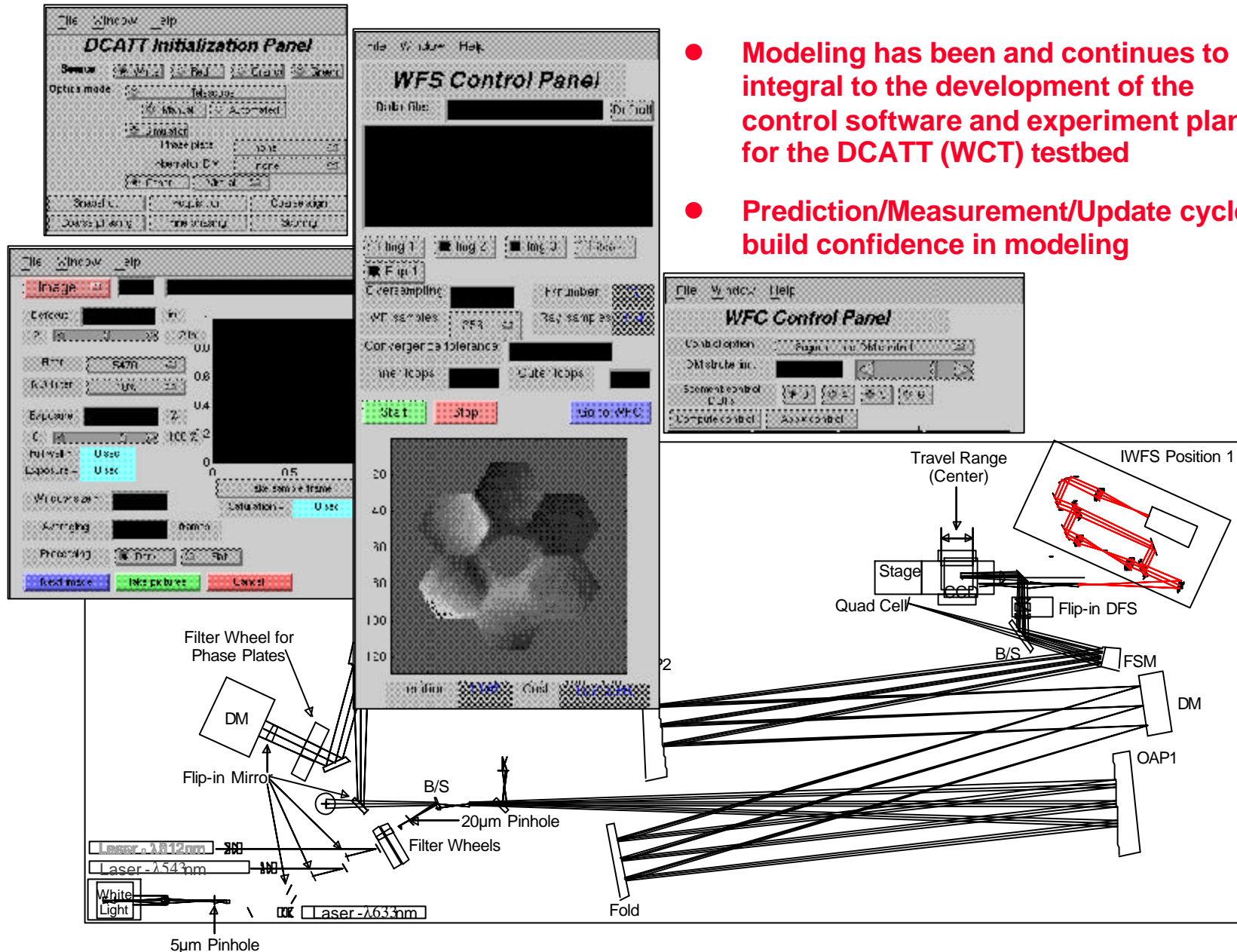


- Return to the notion of a broader meaning for the word integrated...
- Modeling should be thoroughly *integrated* into the complete systems engineering organization/process/mindset
  - For an effort above a certain size, this almost certainly requires a team leader operating at the system level, not a discipline lead doing double-duty
  - Lead analyst needs to plan, communicate, resolve issues, maintain ultimate insight, enforce discipline on process
  - Make it clear what modeling can do
  - Make it clear what modeling cannot do (limitations, uncertainties)
  - Identify needs for modeling to be a success (schedule, manpower, budget, validation and verification methods)
  - Involve key project personnel in a rigorous model validation process
  - Establish regular and frequent communication (peer reviews, telecons, etc.)





# Things we do well: Exploit Testbeds at Every Opportunity



- Modeling has been and continues to be integral to the development of the control software and experiment plan for the DCATT (WCT) testbed
- Prediction/Measurement/Update cycles build confidence in modeling



## Things **WE** could do better



### *Establish a process for timely model validation...*

**“All models are wrong, some models are useful” (George Box)**

**“An approximate answer to the right question is worth a good deal more than the exact answer to an approximate problem” (John Tukey)**

### *Question/defend the choice of methods & tools...*

**“When the only tool you have is a hammer, then every problem begins to look like a nail” (Abraham Maslow)**

### *Break the habit of reporting nominal and (so-called) worst-case results; develop efficient methods of rigorous statistical analyses*

**“Statistics in the hands of an engineer are like a lamppost to a drunk – they're used more for support than illumination” (A. E. Housman)**

**“Numbers are like people – torture them enough and they'll tell you anything” (unattributed)**



# Exploit Information Technology Solutions



- **Collaboration is increasingly essential**
- **Configuration control of models & documents is critical**
- **Avoid, if possible, funneling all analysis through an individual or small cadre of experts – web-accessible models**
- **A disproportionate amount of time can be spent creating Powerpoint presentations in order to collaborate – sometimes unavoidable, but still wasteful**
- **E-mail as a means of communicating can be inefficient**
- **Computer security a concern for HTTP, FTP**
- **Do a better job of making our computers work for us in order to ease the burdens of both the team and the leader**
- **Specifics – segue to Johnny Medina...**